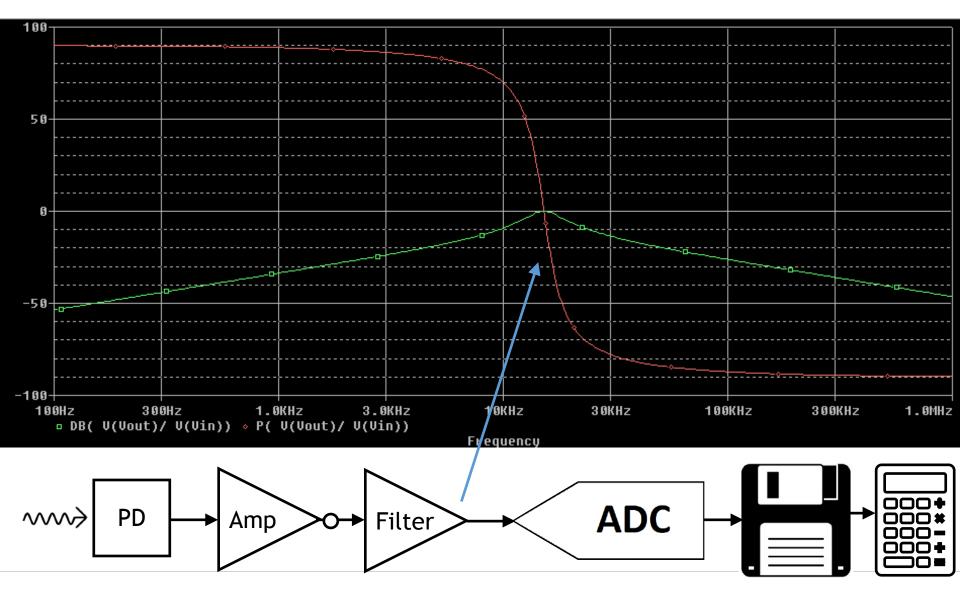
PHYS127AL Lecture 3

David Stuart, UC Santa Barbara Complex impedance, filters, inductors



Review

Review

Input and output impedance & rule for chaining circuit stages Capacitors in time domain: $q=CV \implies I = CdV/dt$

$$V_{\text{in}} \sim I \sim V_{\text{out}}$$

I = C dV/dt

 $V_{out}/R = C d(V_{in}-V_{out})/dt$ If $dV(t)/dt \ll dV_{in}/dt$ then $V_{out}(t) = RC dV_{in}/dt$

Differentiator

$$V_{in} \sim \sqrt{N} \qquad V_{out}$$

$$I = C \, dV/dt$$

$$(V_{in}-V)/R = C \, dV/dt$$

$$V(t) = V_{in} (1 - e^{-t/RC})$$

$$dV = V_{in}(t) \, dt /RC, \quad \text{if } V(t) << V_{in}(t)$$

$$\Rightarrow V(t) = \int V_{in}(t) \, dt /RC$$

Integrator

Outline

- Generalize Ohm's law with complex impedance
- Frequency domain description
- Filters
- Inductors
- Phase diagrams

Ohm's law for capacitors

- We can find an IV relationship for a capacitor. Let's assume that V(t) is sinusoidal; we can then form any AC signal from a Fourier sum of these.
- I'll actually use a cosine for reasons that will become clear later.
- Suppose the voltage across the capacitor is

 $V(t) = V_0 \cos \omega t$

where $\omega = 2\pi f$. Then the current through it is

 $I(t) = C dV(t)/dt = -\omega CV_0 \sin \omega t$

So we have a relation between the magnitudes of V and I

$$|\mathbf{V}| = |\mathbf{I}| (1/\omega \mathbf{C})$$

This is similar to Ohm's law; we can identify *reactance* of a capacitor as $X_C = 1/\omega C$. But it is not the full story because the *phase* of the current differs from the phase of the voltage.

Impedance is the general term for resistance or reactance

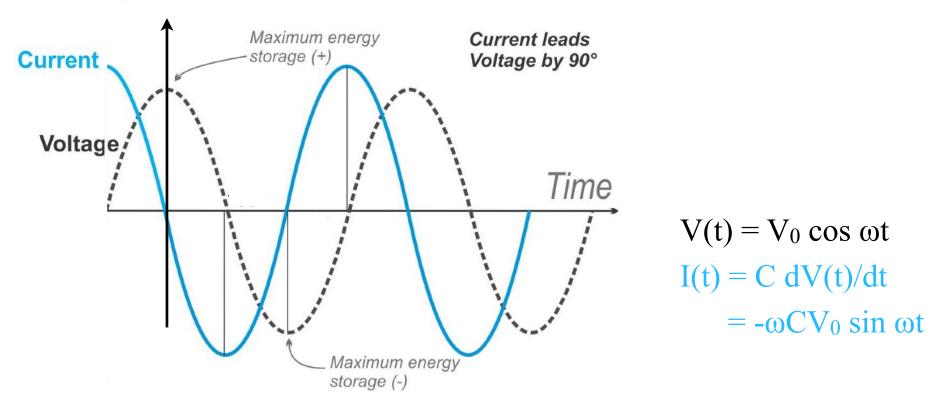
Note that Z is sometimes used for impedance instead of X.

Ohm's law for capacitors

 $|\mathbf{V}| = |\mathbf{I}| (1/\omega \mathbf{C})$

This is similar to Ohm's law, and we can identify $1/\omega C$ as being like the "resistance of a capacitor". But it is not the full story because the *phase* of the current differs from the phase of the voltage.

Ideal Capacitive Circuit Phase Angle

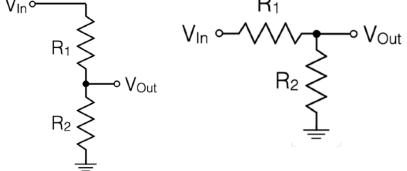


- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.

This simple rule helps us understand this circuit intuitively. $V_{\rm out}$ It is just a voltage divider.

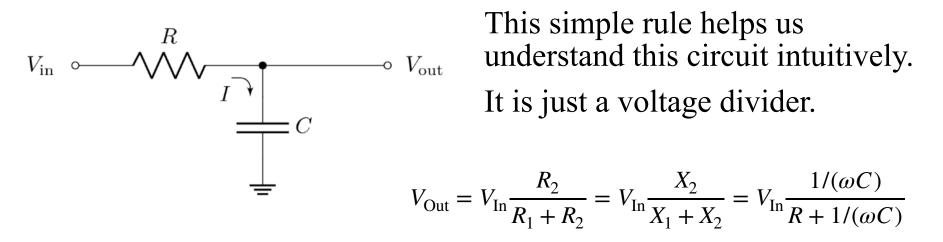
$$V_{\text{Out}} = V_{\text{In}} \frac{R_2}{R_1 + R_2} = V_{\text{In}} \frac{X_2}{X_1 + X_2} = V_{\text{In}} \frac{1/(\omega C)}{R + 1/(\omega C)}$$

 $R_{1} \xrightarrow{H_{1}} V_{\text{In}} \xrightarrow{H_{1}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{In}} \text{ is large } (\cong 1) \text{ if } X_{2} \text{ is } C_{\text{Out}} \xrightarrow{R_{2}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} V_{\text{Out}} \xrightarrow{V_{\text{Out}}} X_{1} \text{ and} \xrightarrow{V_{\text{Out}}} X_{1} \text{ is small} (\cong 0) \text{ if } X_{2} \text{ is } \xrightarrow{U_{1}} \xrightarrow{V_{1}} \xrightarrow{$ V_{Out}/V_{In} is large ($\cong 1$) if X_2 is large small compared to X_1 .



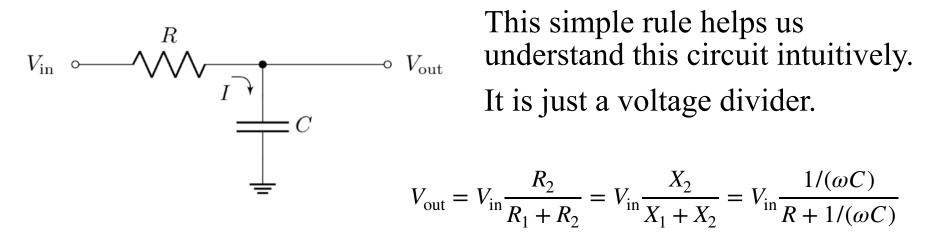
 $V_{\rm in}$ \sim

- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.



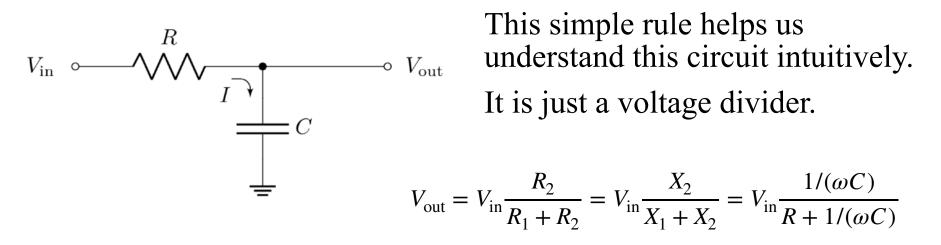
First consider a <u>DC signal</u> at V_{In} , i.e., $\omega=0$. What is V_{out} ?

- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.



First consider a <u>DC signal</u> at V_{in}, i.e., $\omega=0$. What is V_{out}? X_C $\rightarrow\infty$, so V_{out} = V_{in}.

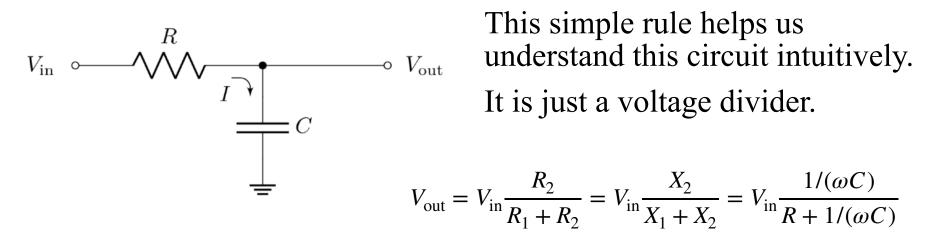
- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.



First consider a <u>DC signal</u> at V_{in}, i.e., $\omega=0$. What is V_{out}? X_C $\rightarrow\infty$, so V_{out} = V_{in}.

Next consider a high frequency AC signal at V_{in} , i.e., $\omega \rightarrow \infty$. What is V_{out} ?

- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.

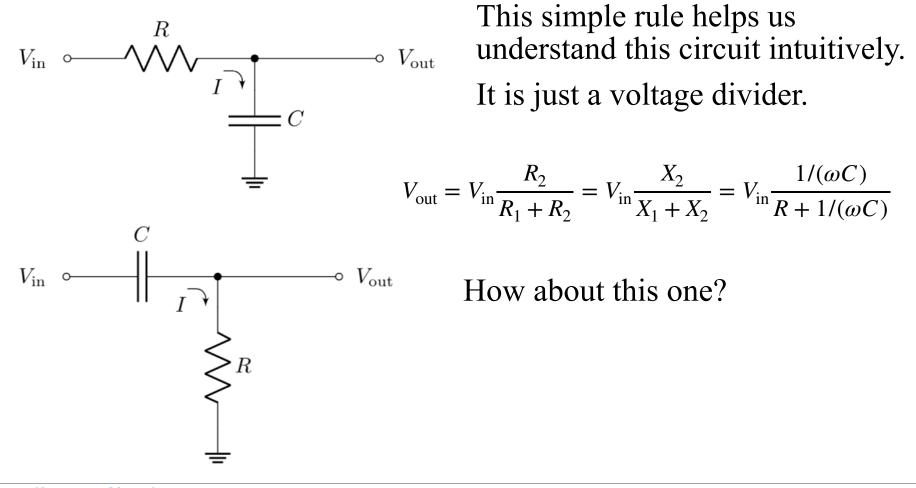


First consider a <u>DC signal</u> at V_{in}, i.e., $\omega=0$. What is V_{out}? X_C=1/(ω C) $\rightarrow\infty$, so V_{out} = V_{in}.

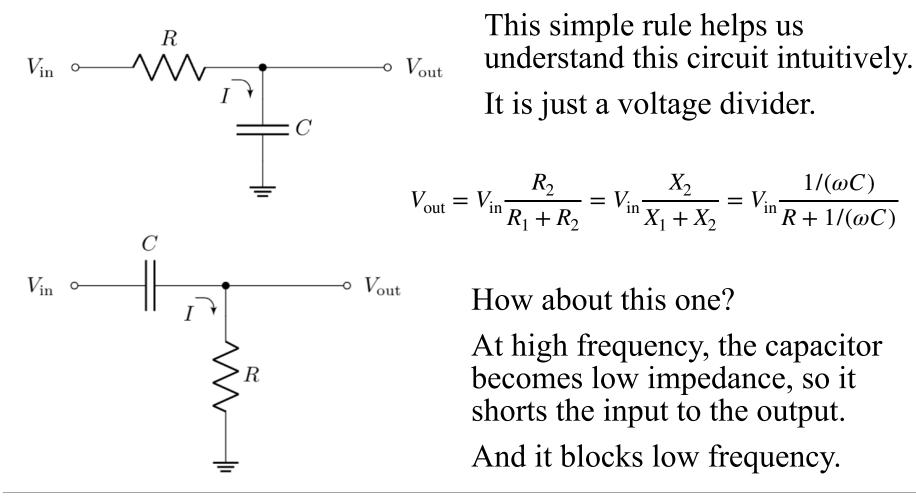
Next consider a <u>high frequency AC signal</u> at V_{in}, i.e., $\omega \rightarrow \infty$. What is V_{out}? $X_C=1/(\omega C)\rightarrow 0$, so V_{out} $\rightarrow 0$.

The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.

Low impedance for high frequency AC and high impedance for DC.



- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency, ω , of the signal.
- Low impedance for high frequency AC and high impedance for DC.



DavidStuart@UCSB.edu Phys127AL Lecture 3: Complex impedance, filters, inductors

Expressing AC signals in complex notation

It simplifies the handling of AC signals to treat them with complex notation, which includes both amplitude and phase. We can do this with Euler's formula.

 $e^{i\theta} = \cos\,\theta + i\,\sin\,\theta$

So we can express $V(t) = V_0 \cos \omega t$ as $V(t) = V_0 e^{i\omega t}$ well the real part is V(t). We already use *i* for a small signal change in current, so in electronics we instead use $j^2 = -1$. (Textbook uses *j*=-*i*.) So we'll represent the voltage as $\widetilde{V}(t) = V_0 e^{j\omega t}$

<u>The tilde reminds us that this is the complex representation.</u> Now calculate the current from I = C dV/dt.

$$\widetilde{I} = C \ d\widetilde{V}/dt = C j \omega V_0 e^{j\omega t} = j \omega C \widetilde{V}$$

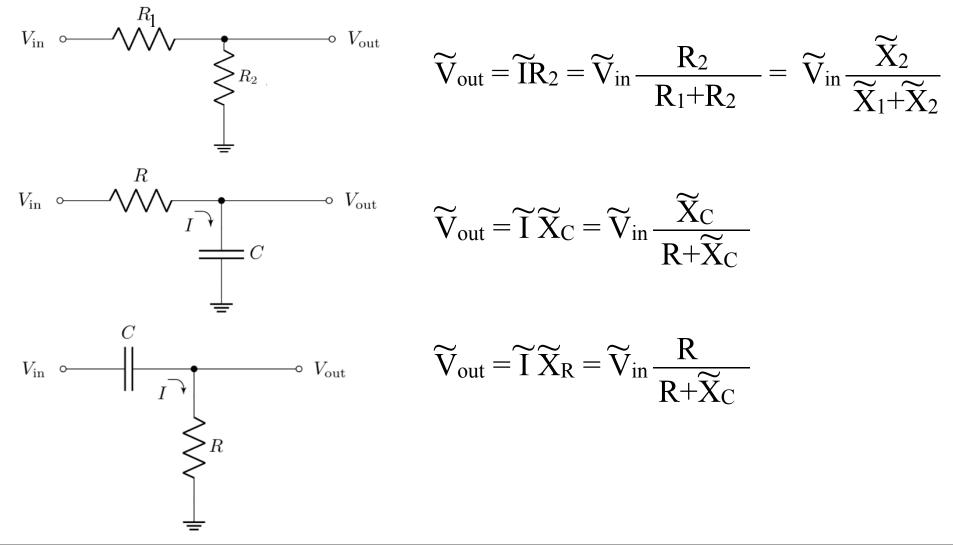
So, we can write an Ohm's law like relation between \widetilde{V} and \widetilde{I} :
$$\widetilde{V} = \widetilde{I} (1/j\omega C) = \widetilde{I} (-j/\omega C) \implies \widetilde{V} = \widetilde{I} \widetilde{X}_C \quad \text{cf} \quad \widetilde{V} = \widetilde{I} \widetilde{X}_R$$

Where the impedance of the capacitor in complex representation is $\widetilde{X}_{C} = -j/\omega C$ cf $\widetilde{X}_{R} = R$ (the -*j* carries information about the phase)

Expressing AC signals in complex notation

This will simplify handling a mix of capacitors and resistors.

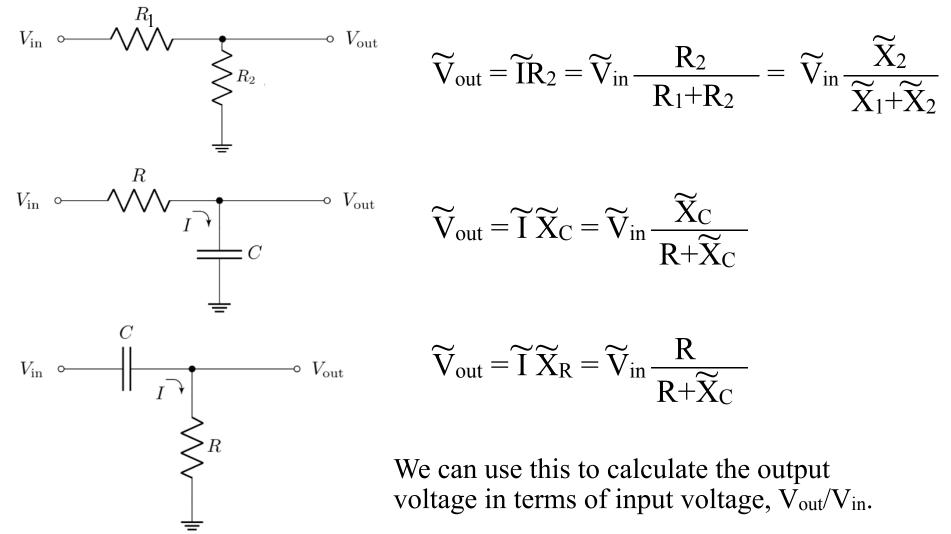
This makes the circuits below just complex voltage dividers.

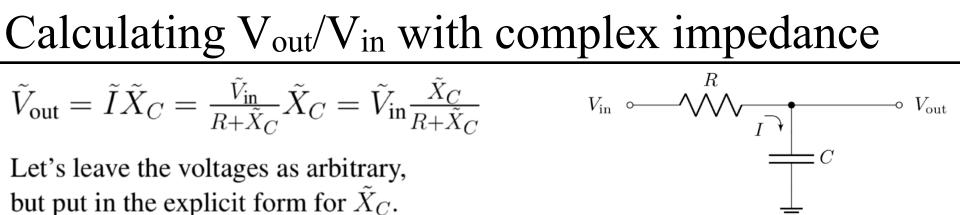


Expressing AC signals in complex notation

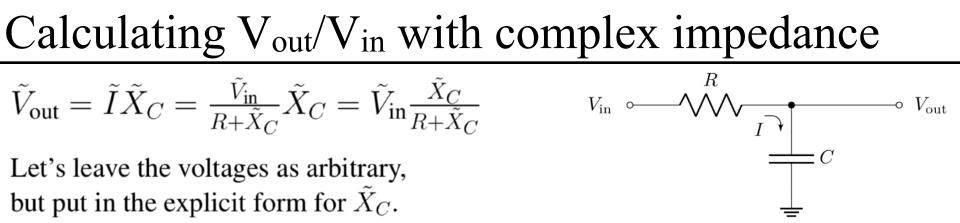
This will simplify handling a mix of capacitors and resistors.

This makes the circuits below just complex voltage dividers.





$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right]$$



$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$

Calculating V_{out}/V_{in} with complex impedance $\tilde{V}_{out} = \tilde{I}\tilde{X}_C = \frac{\tilde{V}_{in}}{R+\tilde{X}_C}\tilde{X}_C = \tilde{V}_{in}\frac{\tilde{X}_C}{R+\tilde{X}_C}$ $V_{in} \sim \sqrt{N}_{I} \xrightarrow{I} C$ Let's leave the voltages as arbitrary, but put in the explicit form for \tilde{X}_C .

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2}$$

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2}$$

$$|\tilde{V}_{\text{out}}| = |\tilde{V}_{\text{in}}| \left| \frac{1 - j\omega RC}{1 + \omega^2 R^2 C^2} \right|$$

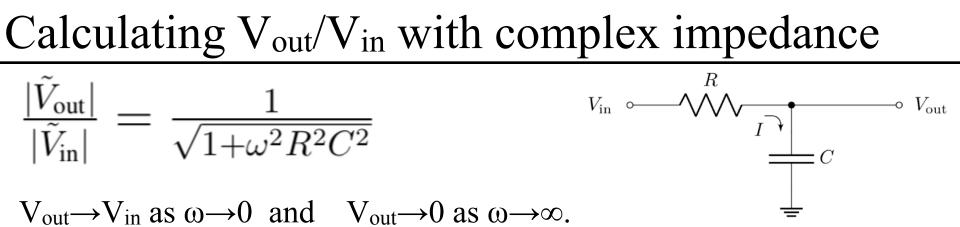
$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \left| \frac{1 - j\omega RC}{1 + \omega^2 R^2 C^2} \right|$$

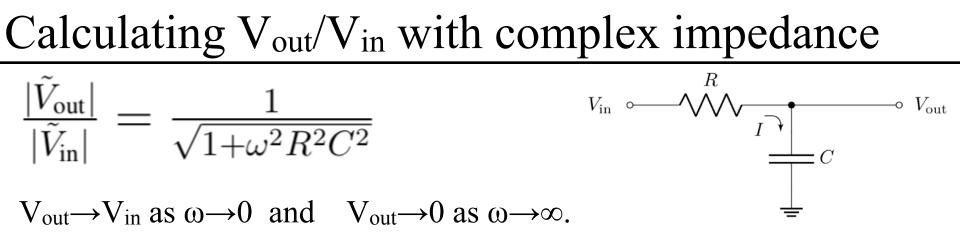
$$\begin{split} \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2} \\ \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2} \end{split}$$

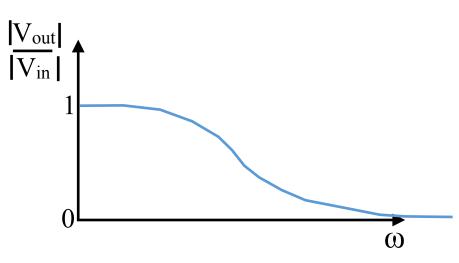
$$|\tilde{V}_{\text{out}}| = |\tilde{V}_{\text{in}}| \left| \frac{1 - j\omega RC}{1 + \omega^2 R^2 C^2} \right|$$

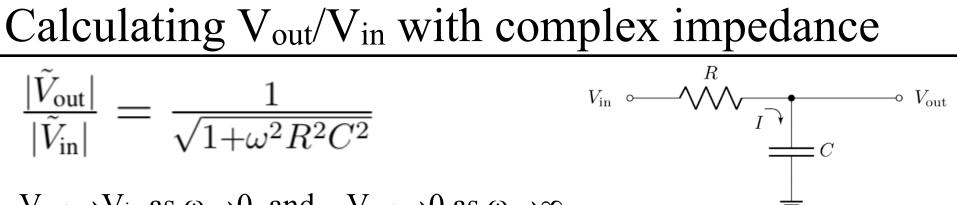
$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \left|\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right| = \sqrt{\left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right] \left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right]^*} = \sqrt{\left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right] \left[\frac{1+j\omega RC}{1+\omega^2 R^2 C^2}\right]} \\ \frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \sqrt{\frac{1+\omega^2 R^2 C^2}{(1+\omega^2 R^2 C^2)^2}} = \frac{\sqrt{1+\omega^2 R^2 C^2}}{1+\omega^2 R^2 C^2} = \frac{1}{\sqrt{1+\omega^2 R^2 C^2}}$$

This is the response function for the circuit, and it is frequency dependent through $\omega = 2\pi f$.

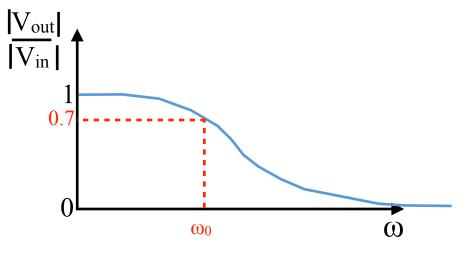








 $V_{out} \rightarrow V_{in} \text{ as } \omega \rightarrow 0 \text{ and } V_{out} \rightarrow 0 \text{ as } \omega \rightarrow \infty.$

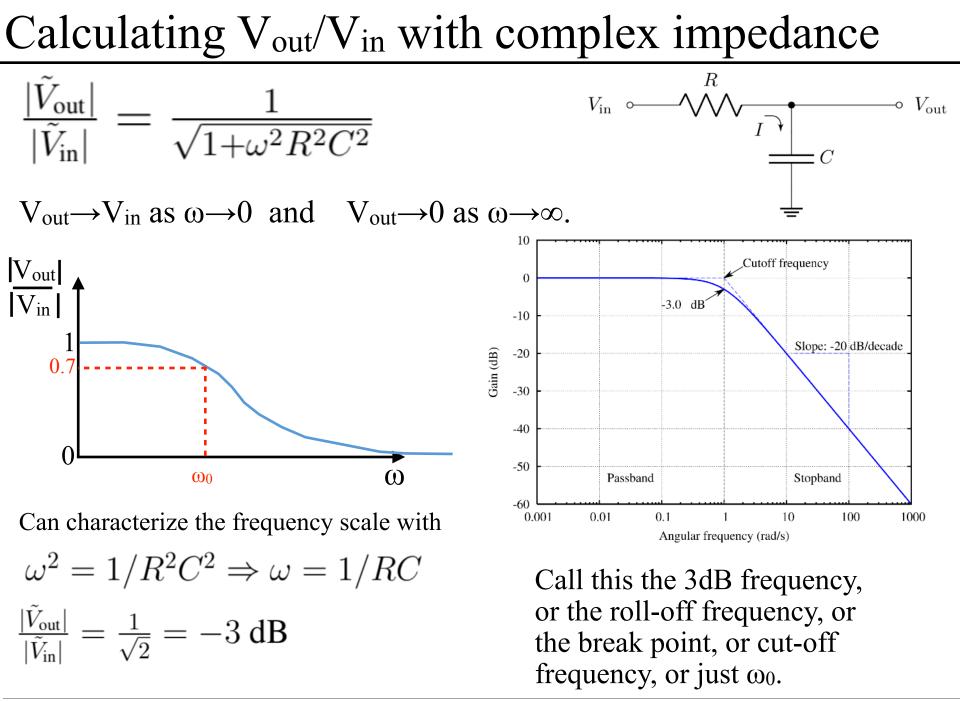


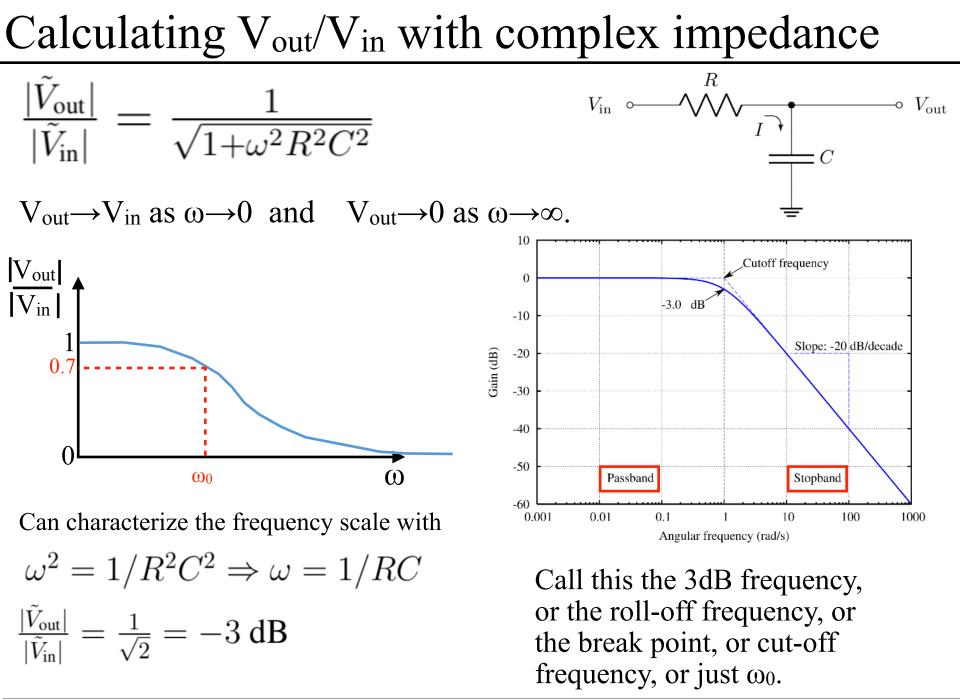
Can characterize the frequency scale with

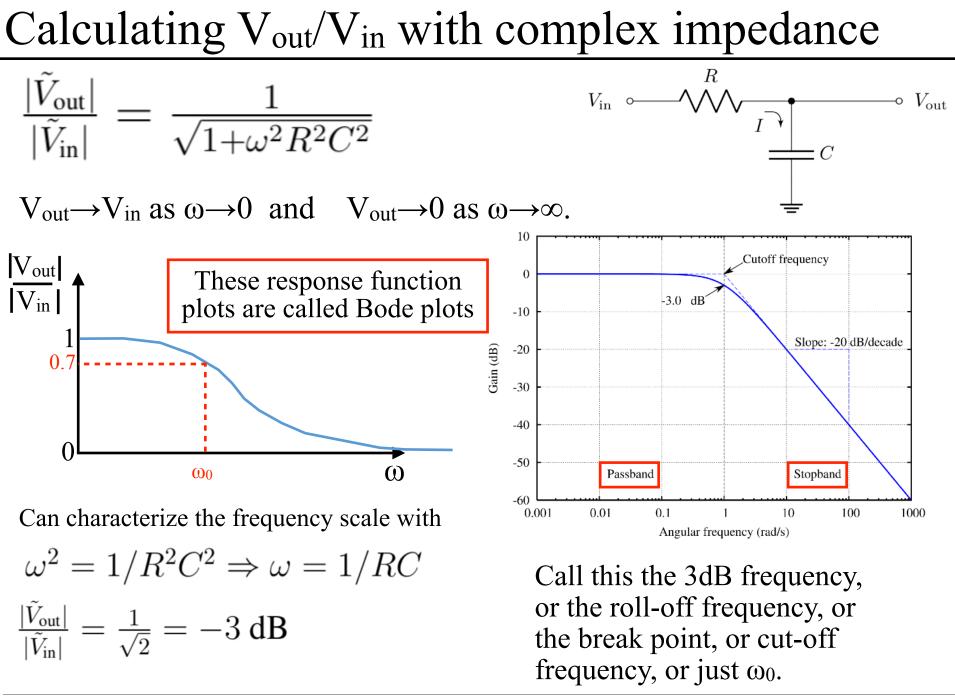
$$\omega^2 = 1/R^2 C^2 \Rightarrow \omega = 1/RC$$

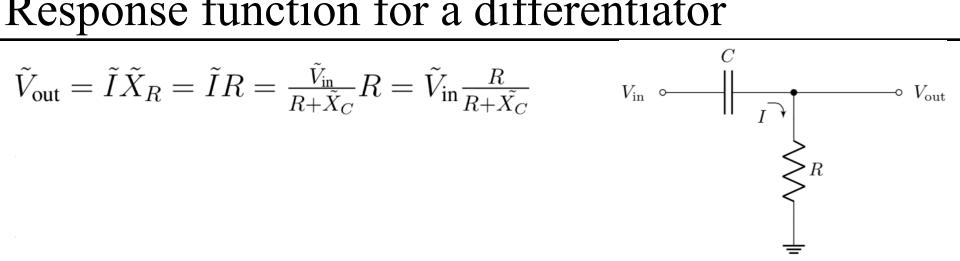
$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \frac{1}{\sqrt{2}} = -3 \text{ dB}$$

Call this the 3dB frequency, or the roll-off frequency, or the break point, or cut-off frequency, or just ω_0 .

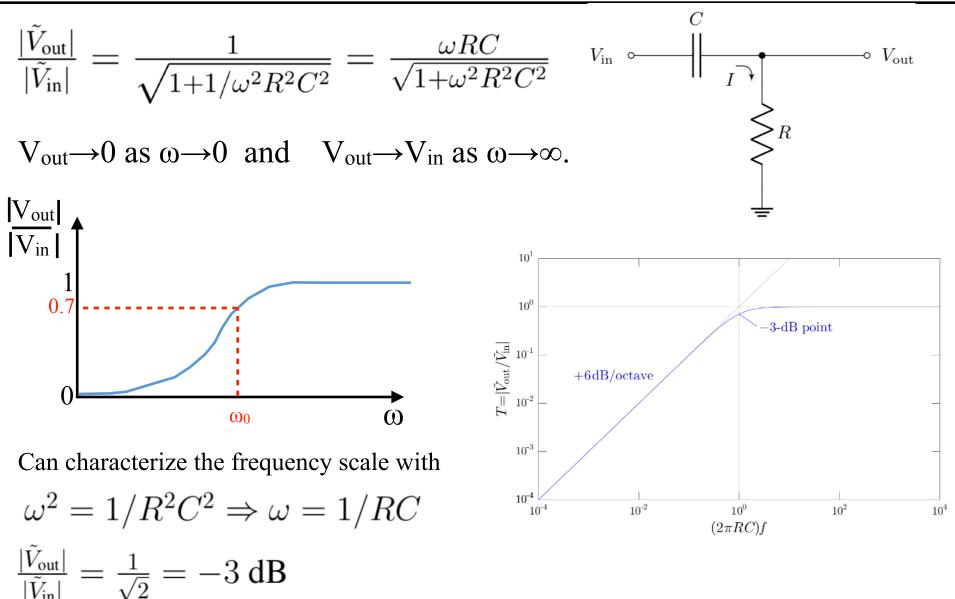




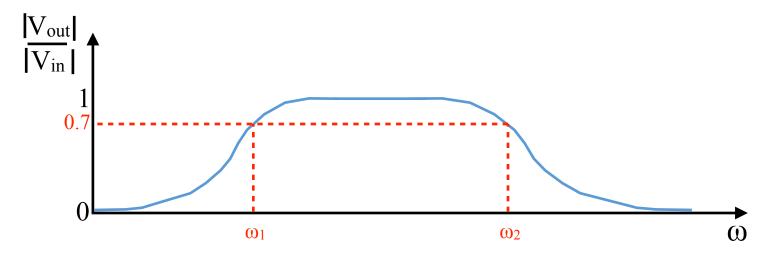




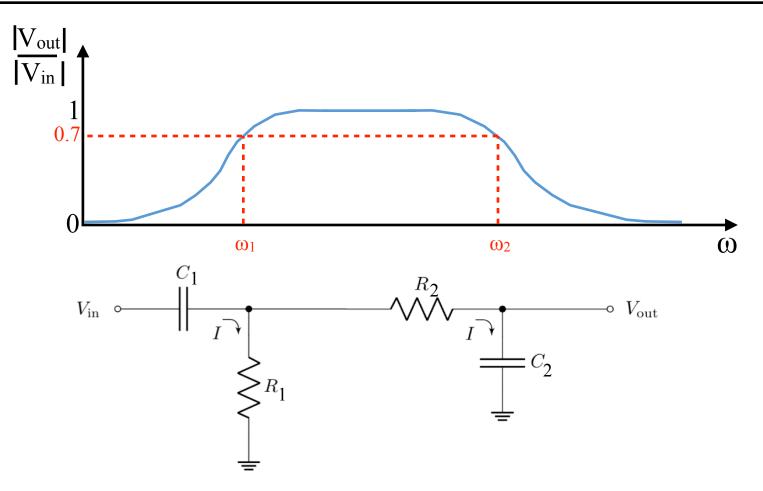
$$\begin{split} \tilde{V}_{\text{out}} &= \tilde{I}\tilde{X}_R = \tilde{I}R = \frac{\tilde{V}_{\text{in}}}{R + \tilde{X}_C} R = \tilde{V}_{\text{in}} \frac{R}{R + \tilde{X}_C} \qquad v_{\text{in}} \circ \overbrace{\qquad}^C \\ \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \left[\frac{R}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{R}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] \\ \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \frac{R^2 + jR/\omega C}{R^2 + 1/\omega^2 C^2} = \tilde{V}_{\text{in}} \frac{1 + j/\omega R C}{1 + 1/\omega^2 R^2 C^2} \\ \left| \tilde{V}_{\text{out}} \right| &= \left| \tilde{V}_{\text{in}} \right| \left| \frac{1 + j\omega R C}{1 + \omega^2 R^2 C^2} \right| \\ \frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} &= \left| \frac{1 + j/\omega R C}{1 + 1/\omega^2 R^2 C^2} \right| = \sqrt{\left[\frac{1 + j/\omega R C}{1 + 1/\omega^2 R^2 C^2} \right] \left[\frac{1 - j/\omega R C}{1 + 1/\omega^2 R^2 C^2} \right]} \\ \frac{|\tilde{V}_{\text{oul}}|}{|\tilde{V}_{\text{in}}|} &= \sqrt{\frac{1 + 1/\omega^2 R^2 C^2}{(1 + 1/\omega^2 R^2 C^2)^2}} = \frac{\sqrt{1 + 1/\omega^2 R^2 C^2}}{1 + 1/\omega^2 R^2 C^2} = \frac{1}{\sqrt{1 + 1/\omega^2 R^2 C^2}} \\ \end{array}$$



How would you make a band-pass filter?



How would you make a band-pass filter?

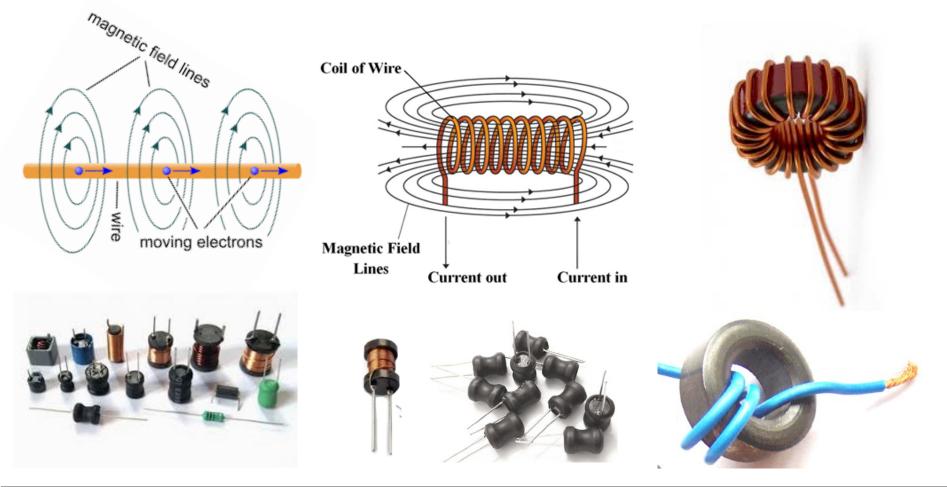


Often called a CR-RC filter.

Remove DC offset and remove high frequency noise.

Inductors

A capacitor stored energy in the electric field, in the voltage. I = C dV/dtAn inductor stores energy in the magnetic field, the current. V = L dI/dtAny wire has inductance. A coil has more. An iron core coil even more.



Inductors

Unit of inductance is the Henry = $1 \text{ Vs/A} = \Omega \text{s}$ (since V = L dI/dt). Symbol looks like a coil. Some special symbols, but simple one is fine.

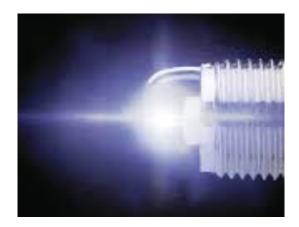
Inductor Symbols Air Core Iron Core Ferrite Variable Core Core

Typical values are µH to mH.

Parasitic inductance comes from any wire. thinner and longer wires have higher L. A 1 mm diameter wire has L = O(1) nH/mm.

Inductive sparks

Since V = L dI/dt something that changes the current quickly will cause a large voltage across the inductor. A vacuum cleaner motor is mostly an inductor and will spark at the power cord if you unplug it.



Inductive sparks

Since V = L dI/dt something that changes the current quickly will cause a large voltage across the inductor. A vacuum cleaner motor is mostly an inductor and will spark at the power cord if you unplug it.



Impedance of an inductor

We can again use the complex representation of V and I to determine the impedance (reactance) of an inductor from V = L dI/dt. Represent I as

$$\widetilde{I}(t) = I_0 e^{j\omega t}$$

So the voltage is

$$\widetilde{\mathbf{V}} = \mathbf{L} j \boldsymbol{\omega} \mathbf{I}_0 \, \mathbf{e}^{j \boldsymbol{\omega} \mathbf{t}} = j \boldsymbol{\omega} \mathbf{L} \widetilde{\mathbf{I}}$$

So, we can write an Ohm's law like relation between V and I: $\widetilde{V} = \widetilde{I} (j\omega L) \implies \widetilde{V} = \widetilde{I} \widetilde{X}_L$

where the impedance of the inductor is

$$\widetilde{X}_L = j\omega L$$
 of $\widetilde{X}_R = R$ and $\widetilde{X}_C = -j/\omega C$

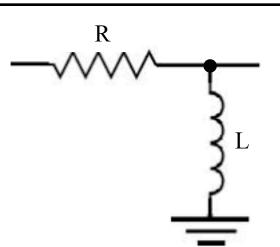
Different frequency dependence from capacitor. Sign difference corresponds to a different phase response

Impedance of an inductor

- $\widetilde{\mathbf{X}}_{\mathrm{L}} = j\omega \mathbf{L}$
- Low impedance at DC; just the normal resistance that contributes.
- Impedance goes to infinity at high frequency.
 - Keep wires short in high frequency circuits.
 - Can block high frequency noise with a simple inductor (ferrite bead).



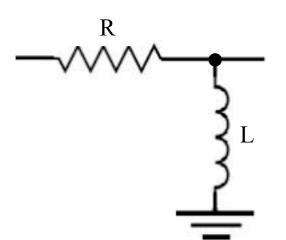
- Let's calculate the transfer function for an RL filter. But first, is it high or low pass?
- Hint: Think of the voltage divider equation.



 $\widetilde{\mathbf{X}}_{\mathrm{L}} = j\omega \mathbf{L}$

- Let's calculate the transfer function for an RL filter. But first, is it high or low pass?
- Hint: Think of the voltage divider equation.
- At low ω , $X_L \rightarrow 0$ so $V_{out} \rightarrow 0$

And $X_L \rightarrow \infty$ as $\omega \rightarrow \infty$ so $V_{out} \rightarrow V_{in}$

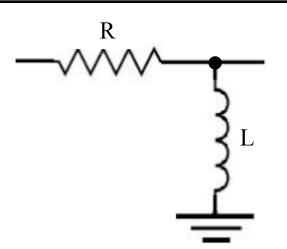


 $\widetilde{X}_L = j\omega L$

- Let's calculate the transfer function for an RL filter. But first, is it high or low pass?
- Hint: Think of the voltage divider equation.
- At low ω , $X_L \rightarrow 0$ so $V_{out} \rightarrow 0$

And $X_L \rightarrow \infty$ as $\omega \rightarrow \infty$ so $V_{out} \rightarrow V_{in}$

$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_L = \tilde{I}j\omega L = \tilde{V}_{\text{in}}\frac{j\omega L}{R+j\omega L}$$



 $\widetilde{X}_L = j\omega L$

- Let's calculate the transfer function for an RL filter. But first, is it high or low pass?
- Hint: Think of the voltage divider equation.
- At low ω , X_L $\rightarrow 0$ so V_{out} $\rightarrow 0$

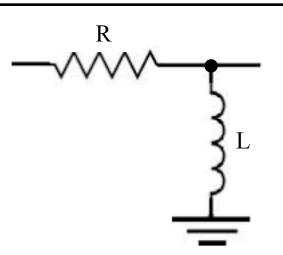
And $X_L \rightarrow \infty$ as $\omega \rightarrow \infty$ so $V_{out} \rightarrow V_{in}$

$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_L = \tilde{I}j\omega L = \tilde{V}_{\text{in}}\frac{j\omega L}{R+j\omega L}$$

$$\frac{\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \frac{\omega L}{\sqrt{R^2 + \omega^2 L^2}} = \frac{1}{\sqrt{1 + R^2/\omega^2 L^2}}$$

Compare to differentiator:

$$\frac{|\tilde{V}_{\rm out}|}{|\tilde{V}_{\rm in}|} = \frac{1}{\sqrt{1 + 1/\omega^2 R^2 C^2}} = \frac{\omega RC}{\sqrt{1 + \omega^2 R^2 C^2}}$$

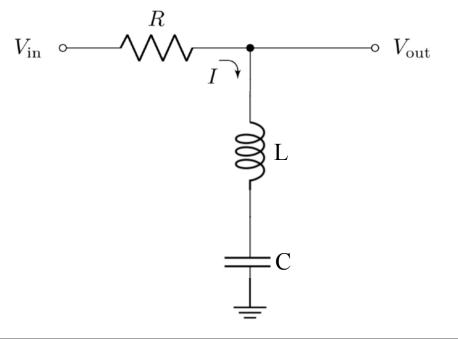


 $\tilde{X}_L = j\omega L$

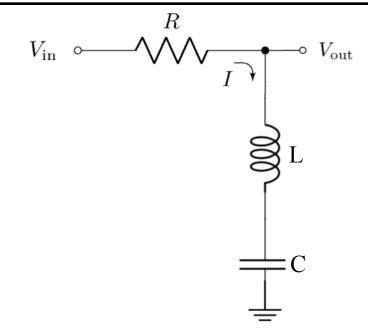
Textbook does this one:

 $V_{\text{in}} \bullet V_{\text{out}}$

I will do this one:



$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_{(L+C)} = \tilde{V}_{\text{in}}\frac{\tilde{X}_{(L+C)}}{\tilde{X}_{(R+L+C)}}$$



$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_{(L+C)} = \tilde{V}_{\text{in}}\frac{\tilde{X}_{(L+C)}}{\tilde{X}_{(R+L+C)}}$$

First we need to know how to combine impedances. They all add like resistance.

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{j\omega L - j/\omega C}{R + j\omega L - j/\omega C} = \tilde{V}_{\text{in}} \frac{j(\omega L - 1/\omega C)}{R + j(\omega L - 1/\omega C)} = \tilde{V}_{\text{in}} \frac{jz}{R + jz}$$

 $V_{\rm out}$

R

 $V_{\rm in}$ \sim

$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_{(L+C)} = \tilde{V}_{\text{in}}\frac{\tilde{X}_{(L+C)}}{\tilde{X}_{(R+L+C)}}$$

First we need to know how to combine impedances. They all add like resistance.

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{j\omega L - j/\omega C}{R + j\omega L - j/\omega C} = \tilde{V}_{\text{in}} \frac{j(\omega L - 1/\omega C)}{R + j(\omega L - 1/\omega C)} = \tilde{V}_{\text{in}} \frac{jz}{R + jz}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{jz}{R + jz} \left[\frac{R - jz}{R - jz} \right] = \tilde{V}_{\text{in}} \frac{z^2 + jRz}{R^2 + z^2} = \tilde{V}_{\text{in}} z \frac{z + jR}{R^2 + z^2}$$

$$\frac{|V_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = z\sqrt{\frac{z^2 + R^2}{(R^2 + z^2)^2}} = \frac{z}{\sqrt{z^2 + R^2}} = \frac{1}{\sqrt{1 + R^2/z^2}}$$

$$\frac{|V_{\text{out}}|}{|\tilde{V}_{\text{in}}|} \to 0 \text{ when } z = \omega L - 1/\omega C \to 0$$

$$\Rightarrow \omega_0 = 1/\sqrt{LC}$$

 $V_{\rm out}$

R

 $V_{\rm in}$ \sim

$$\tilde{V}_{\text{out}} = \tilde{I}\tilde{X}_{(L+C)} = \tilde{V}_{\text{in}}\frac{\tilde{X}_{(L+C)}}{\tilde{X}_{(R+L+C)}}$$

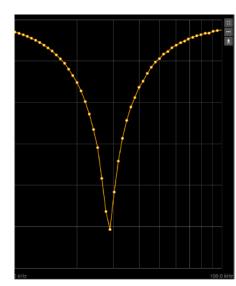
First we need to know how to combine impedances. They all add like resistance.

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{j\omega L - j/\omega C}{R + j\omega L - j/\omega C} = \tilde{V}_{\text{in}} \frac{j(\omega L - 1/\omega C)}{R + j(\omega L - 1/\omega C)} = \tilde{V}_{\text{in}} \frac{jz}{R + jz}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{jz}{R + jz} \left[\frac{R - jz}{R - jz} \right] = \tilde{V}_{\text{in}} \frac{z^2 + jRz}{R^2 + z^2} = \tilde{V}_{\text{in}} z \frac{z + jR}{R^2 + z^2}$$

$$\frac{|V_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = z\sqrt{\frac{z^2 + R^2}{(R^2 + z^2)^2}} = \frac{z}{\sqrt{z^2 + R^2}} = \frac{1}{\sqrt{1 + R^2/z^2}}$$

$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} \to 0 \text{ when } z = \omega L - 1/\omega C \to 0$$

$$\Rightarrow \omega_0 = 1/\sqrt{LC}$$



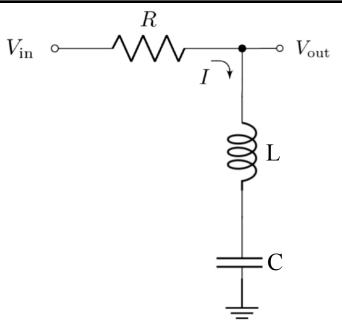
R

 $V_{\rm in}$ \sim

 $V_{\rm out}$

We could have deduced this more simply.

The V_{out} goes to zero when the impedance of the LC leg goes to zero. That is when it shorts the output to ground.

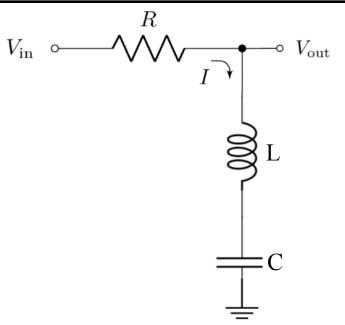


We could have deduced this more simply.

The V_{out} goes to zero when the impedance of the LC leg goes to zero. That is when it shorts the output to ground.

$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} \to 0 \text{ when } z = \omega L - 1/\omega C \to 0$$

$$\Rightarrow \omega_0 = 1/\sqrt{LC}$$



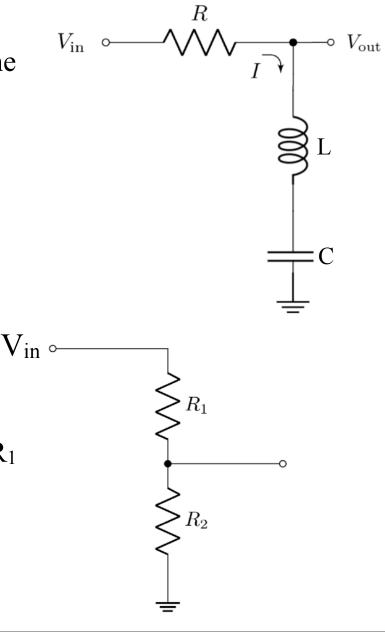
We could have deduced this more simply.

The V_{out} goes to zero when the impedance of the LC leg goes to zero. That is when it shorts the output to ground.

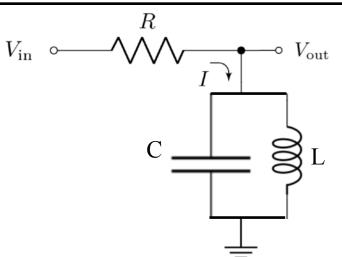
$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} \to 0 \text{ when } z = \omega L - 1/\omega C \to 0$$

$$\Rightarrow \omega_0 = 1/\sqrt{LC}$$

This is the same as a resistive voltage divider, smaller R_2 makes V_{out} go to zero and smaller R_1 makes V_{out} go to V_{in} .

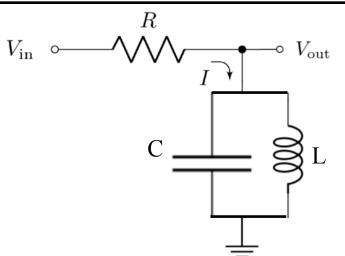


What about this one?



What about this one?

Maximized when C||L is largest.



What about this one?

Maximized when C||L is largest.

$$\tilde{X}_{\mathbf{L}\parallel\mathbf{C}} = \frac{\tilde{X}_{\mathbf{L}}\tilde{X}_{\mathbf{C}}}{\tilde{X}_{\mathbf{L}} + \tilde{X}_{\mathbf{C}}} = \frac{(j\omega L)(-j/\omega C)}{j\omega L - j/\omega C} = \frac{L/C}{j(\omega L - 1/\omega C)} = \frac{-jL/C}{\omega L - 1/\omega C}$$

Maximized at
$$\omega_0 = 1/\sqrt{LC}$$

Resonance at that frequency.

 $V_{\rm out}$

R

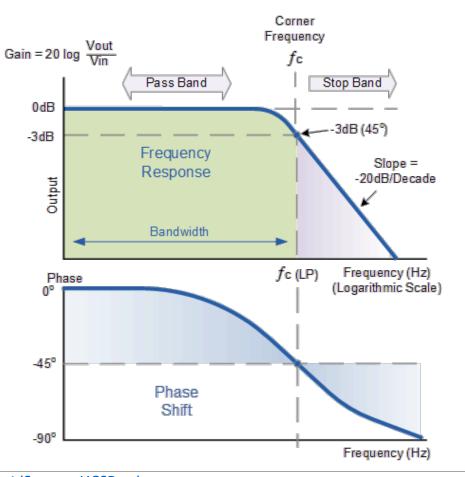
 $V_{\rm in}$ \circ

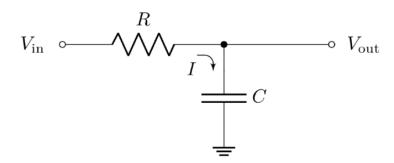
Phase

We saw that current was out of phase with voltage in a capacitor.

So we expect V_{out} and V_{in} to be out of phase.

There is a phase version of the Bode plot.



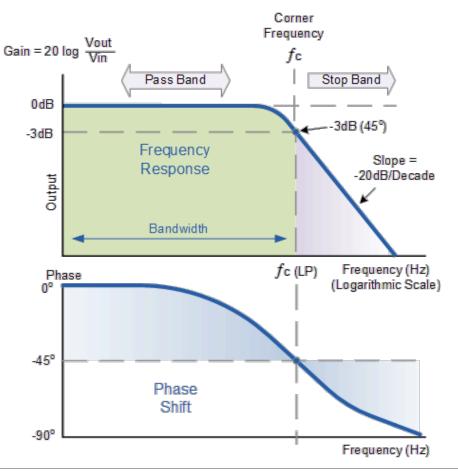


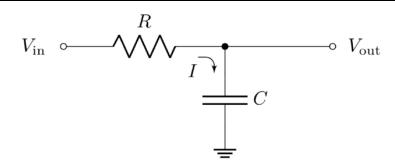
Phase

We saw that current was out of phase with voltage in a capacitor.

So we expect V_{out} and V_{in} to be out of phase.

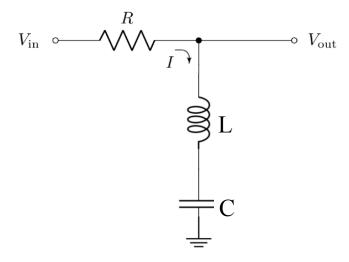
There is a phase version of the Bode plot.



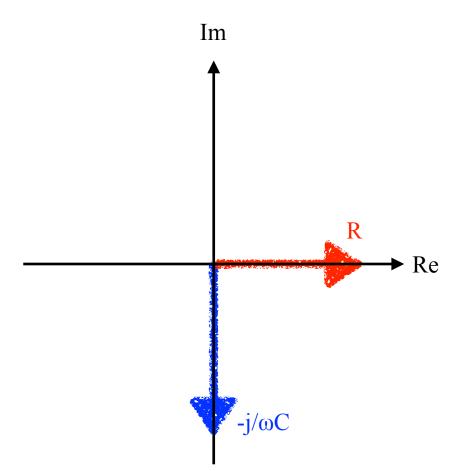


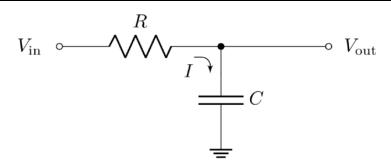
How do we calculate that shift?

What about more complex circuits like this?

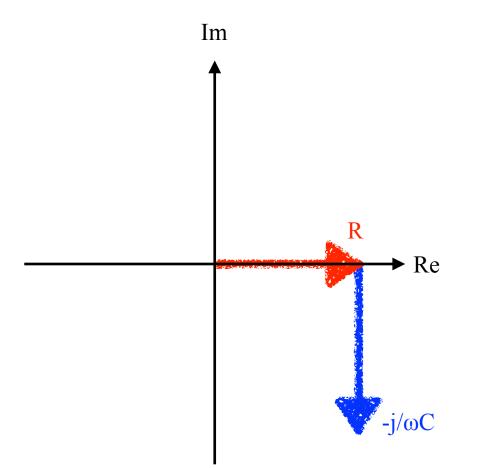


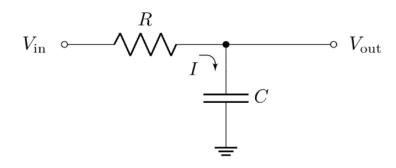
Since the impedance is complex we can draw them in the complex plane.





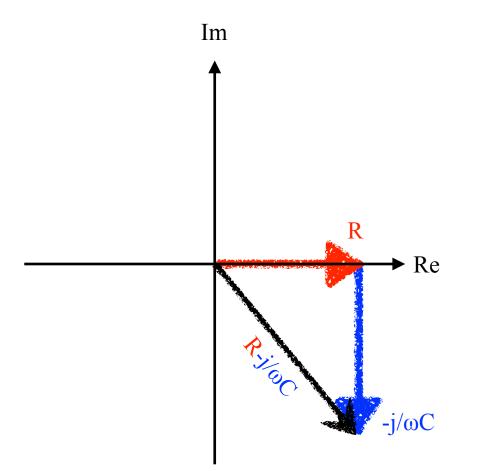
Since the impedance is complex we can draw them in the complex plane.

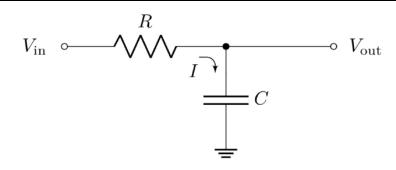




The total impedance is the sum of the R and C contributions, and they add like vectors in the complex plane.

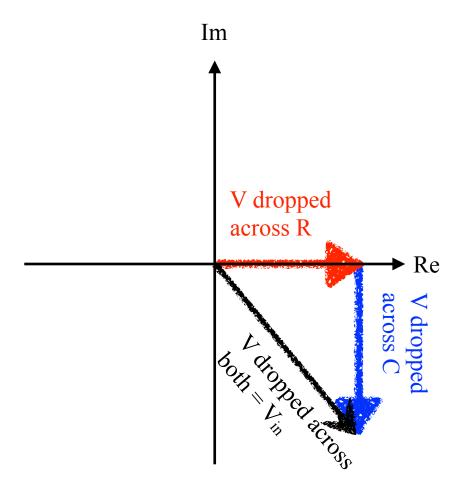
Since the impedance is complex we can draw them in the complex plane.

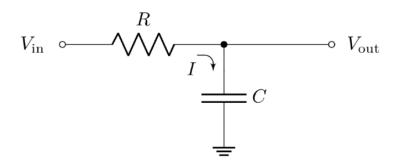




The total impedance is the sum of the R and C contributions, and they add like vectors in the complex plane.

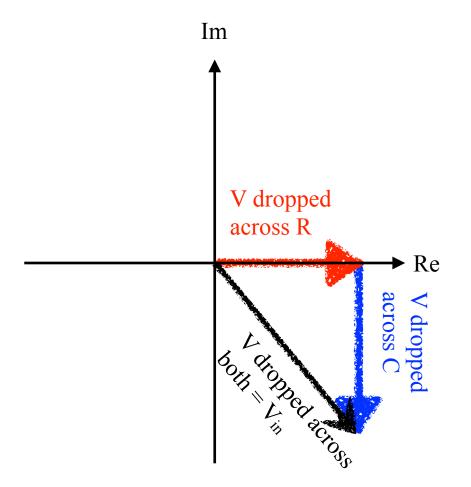
Since the impedance is complex we can draw them in the complex plane.

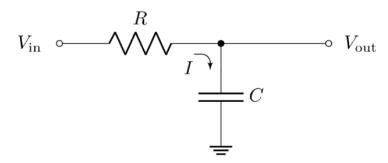




A current flowing through these impedances will drop voltages across them, so this also represents the voltage across these components.

Since the impedance is complex we can draw them in the complex plane.



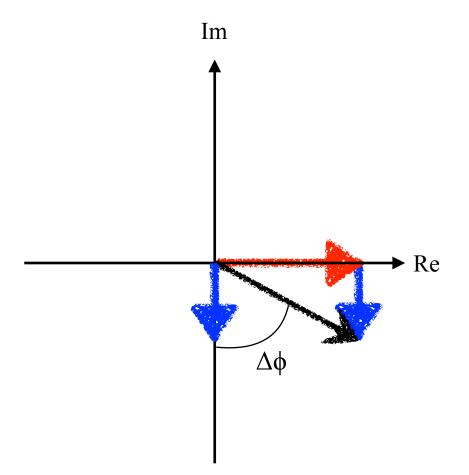


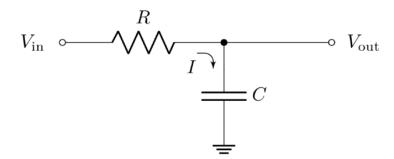
The angle between the vectors is their relative phase.

In $V_0 e^{j\omega t}$ the time dependence corresponds to sweeping the phase around.

Here we care about *relative* phase between voltage dropped across components.

Since the impedance is complex we can draw them in the complex plane.

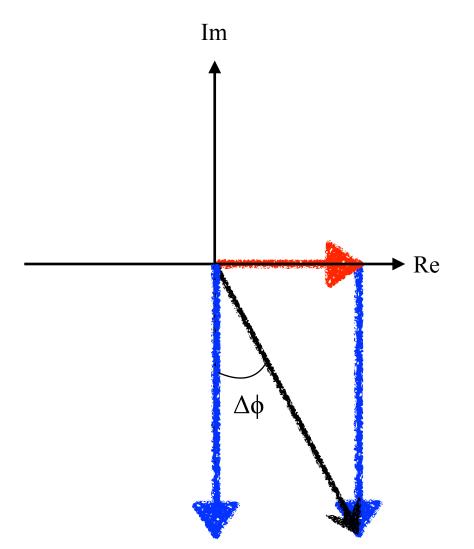


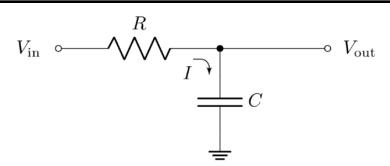


Increasing ω makes $|X_C| = 1/\omega C$ smaller. $V_C \propto 1/\omega$.

Smaller voltage drop across C has larger angle between the C vector, which is V_{out}, and the total vector, which is V_{in}.

Since the impedance is complex we can draw them in the complex plane.

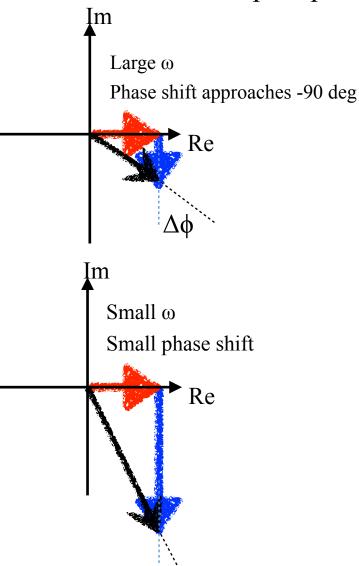


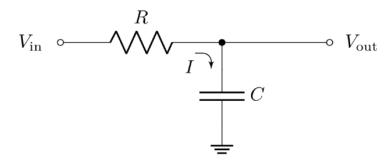


Increasing ω makes $|X_C| = 1/\omega C$ smaller. $V_C \propto 1/\omega$.

Larger voltage drop across C means V_{in} and V_{out} closer together in angle, smaller phase difference.

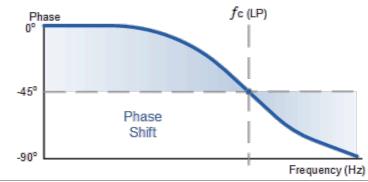
Since the impedance is complex we can draw them in the complex plane.



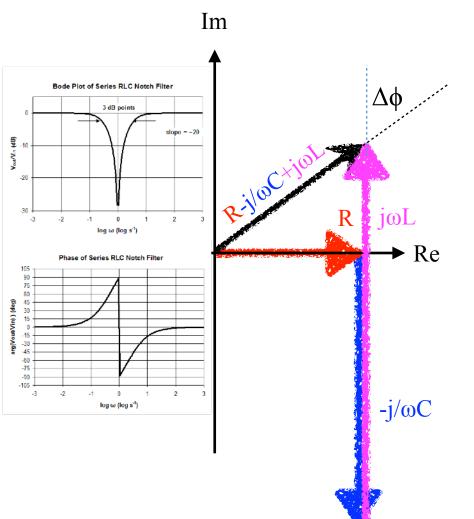


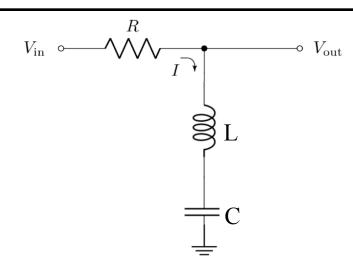
Small voltage drop across C has larger angle between the C vector, which is V_{out}, and the total vector, which is V_{in}.

Larger voltage drop across C means Vin and Vout closer together in angle, smaller phase difference.



Since the impedance is complex we can draw them in the complex plane.





We can analyze an RLC circuit by combining the X_L and X_C .

When X_L and X_C approach exact cancellation, $V_{out} \rightarrow 0$ and phase difference $\rightarrow 90$ degrees. When they deviate in either direction, the phase difference is positive or negative.

$$\omega L - 1/\omega C \to 0$$