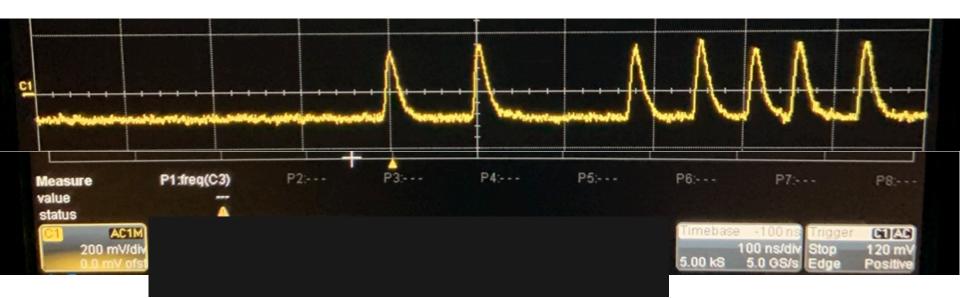
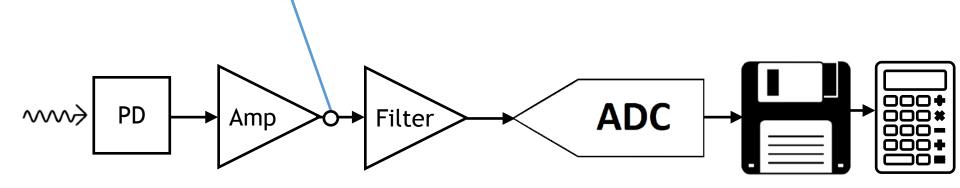
PHYS127AL Lecture 2

David Stuart, UC Santa Barbara Input and output impedance; AC signals; capacitors



Example of an AC signal from a burst of 7 photons over $\sim 1 \mu s$.



Review

Resistors and Ohm's law

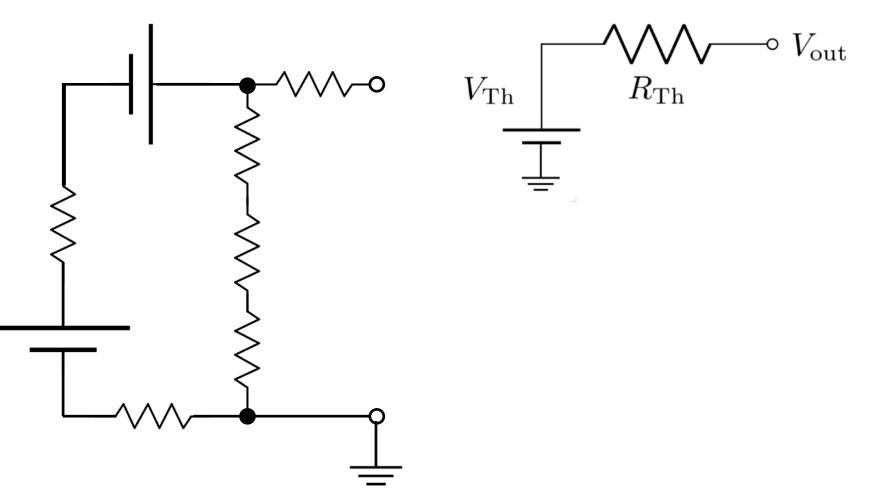
Thevenin and Norton equivalent circuits

Outline

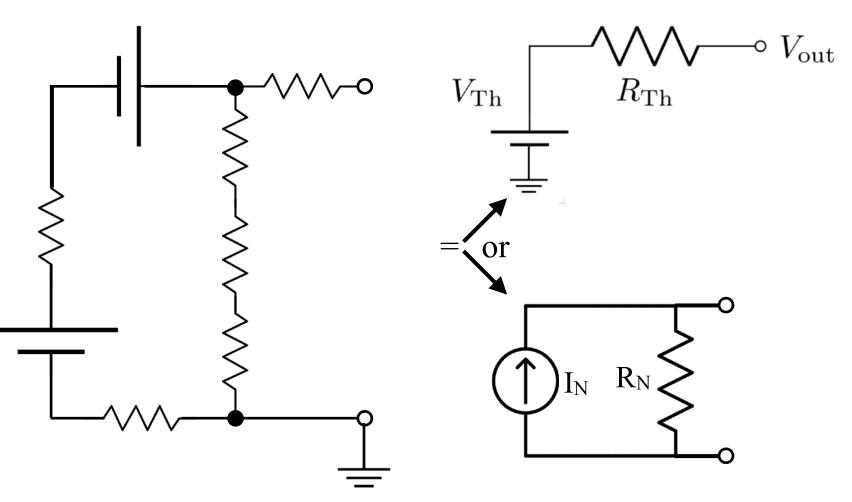
Impedance rule for circuit stages: high input, & low output, impedance Calculating impedance of circuit stages DC vs AC and time dependent signals Capacitors

Thevenin Equivalent Circuits

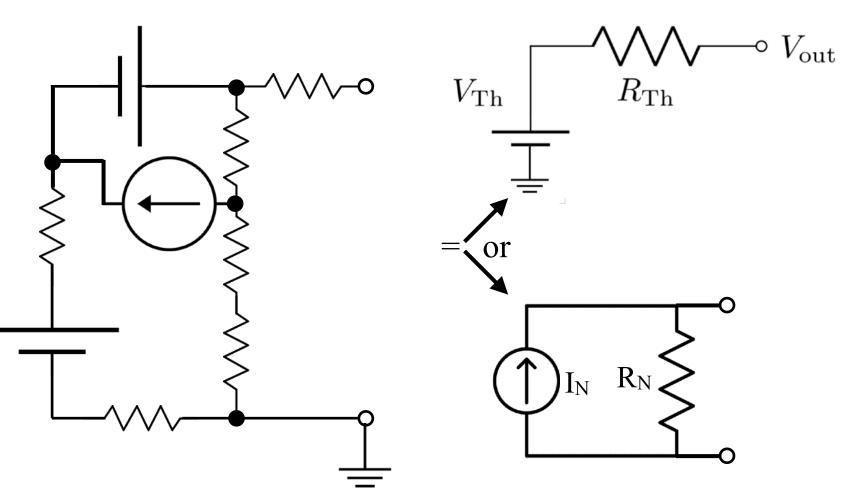
Any mix of voltage sources and resistors can be treated as equivalent to a single voltage source V_{Th} and a single resistor R_{Th} .



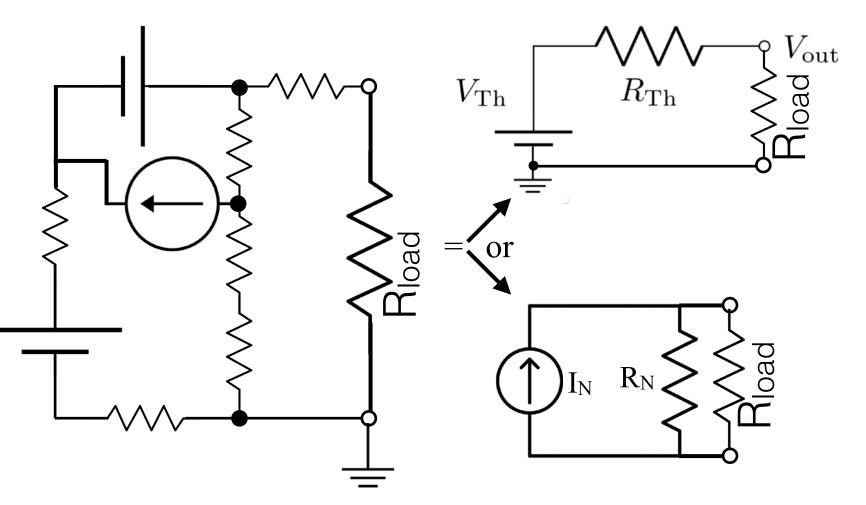
Any mix of voltage sources, current sources, and resistors can be treated as equivalent to a single voltage source V_{Th} and a single resistor R_{Th} , or a single current source I_N and a single resistor R_N .



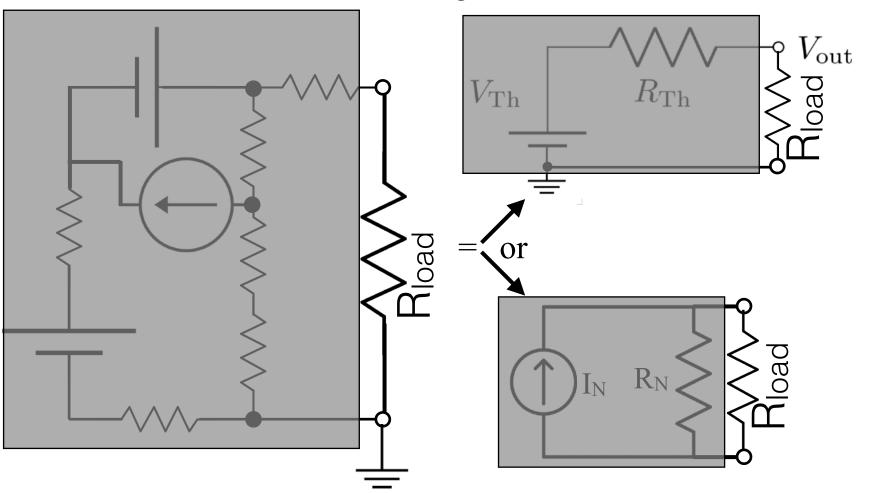
Any mix of voltage sources, current sources, and resistors can be treated as equivalent to a single voltage source V_{Th} and a single resistor R_{Th} , or a single current source I_N and a single resistor R_N .



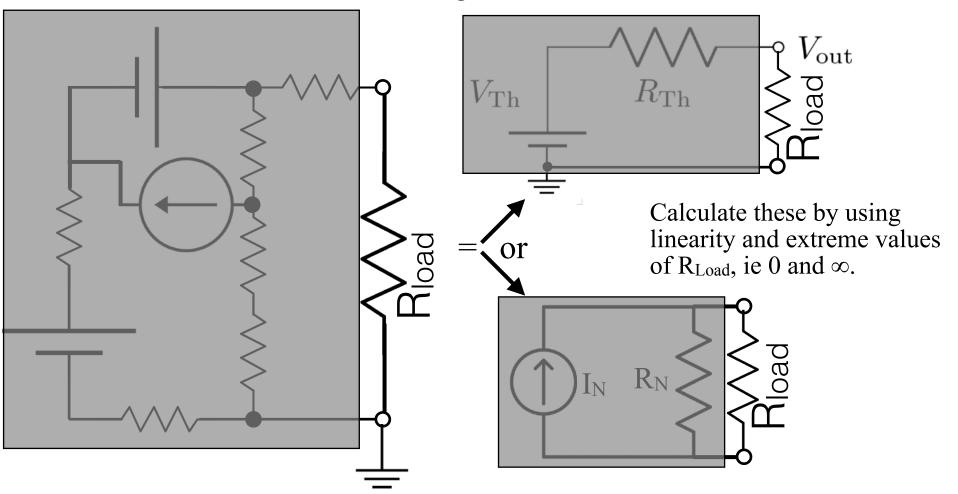
This means that all three behave them same in terms of the IV characteristics when loaded by a resistor. $I(R_{Load})$ and $V(R_{Load})$ is the same for all three circuits.



This means that all three behave them same in terms of the IV characteristics when loaded by a resistor. $I(R_{Load})$ and $V(R_{Load})$ is the same for all three circuits. Indistinguishable black boxes.

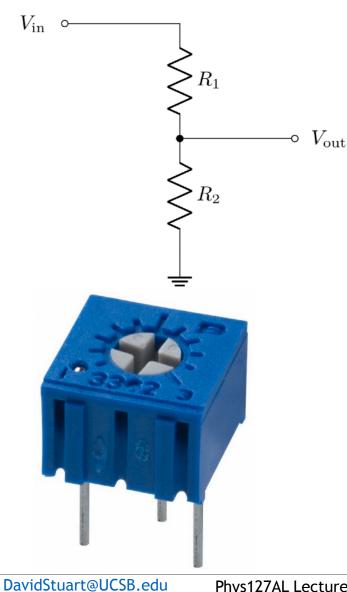


This means that all three behave them same in terms of the IV characteristics when loaded by a resistor. $I(R_{Load})$ and $V(R_{Load})$ is the same for all three circuits. Indistinguishable black boxes.



Voltage divider

This circuit is a voltage divider. We'll use this a lot, and generalize it.

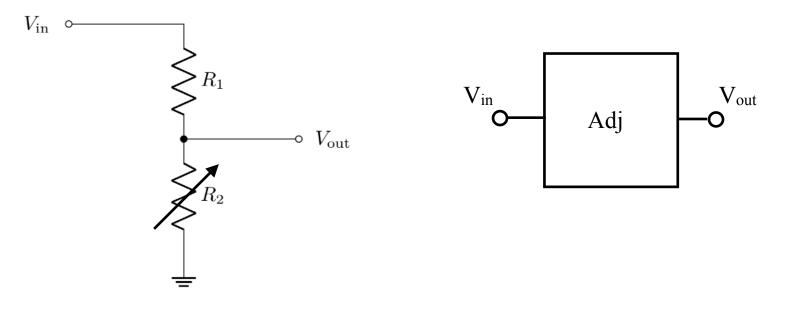


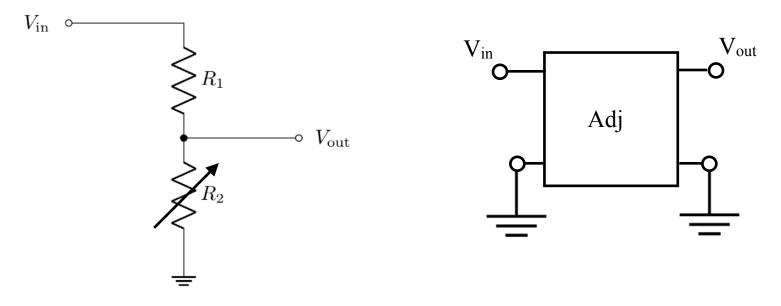
$$V_{out} = IR_2 = [V_{in}/(R_1 + R_2)] R_2 = V_{in} \frac{R_2}{R_1 + R_2}$$

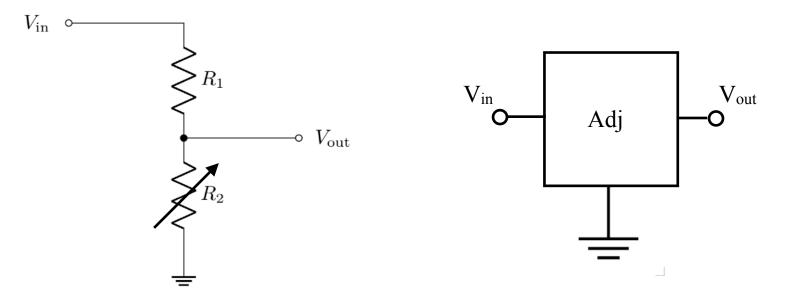
If $R_1 = R_2$ then $V_{out} = \frac{1}{2}V_{in}$

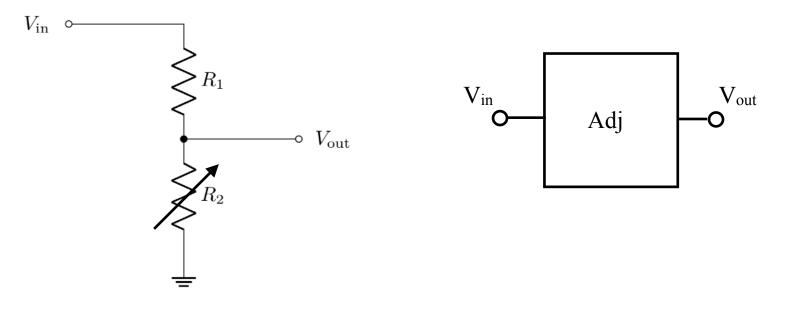
If $R_2 = 10 R_1$ then $V_{out} \approx 0.9 V_{in}$ which is close enough.

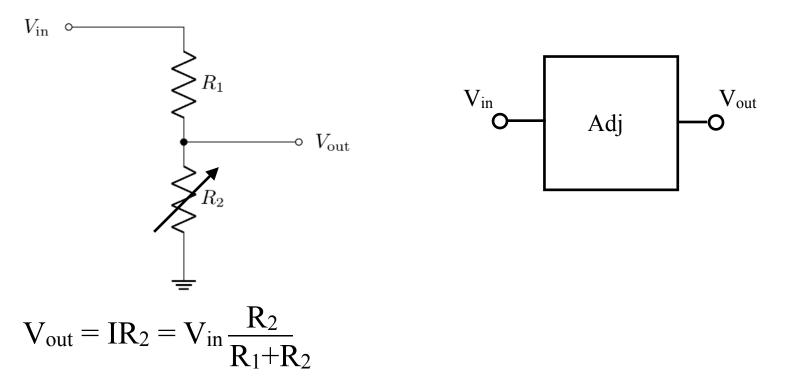
Trimpots used frequently for this to get an adjustable voltage.



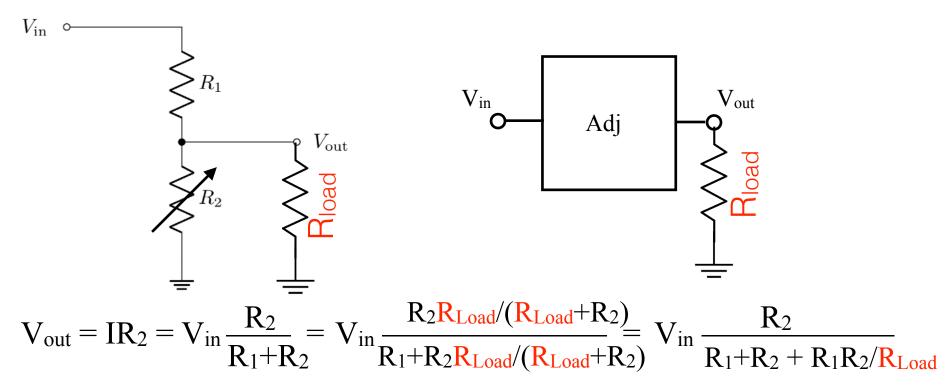






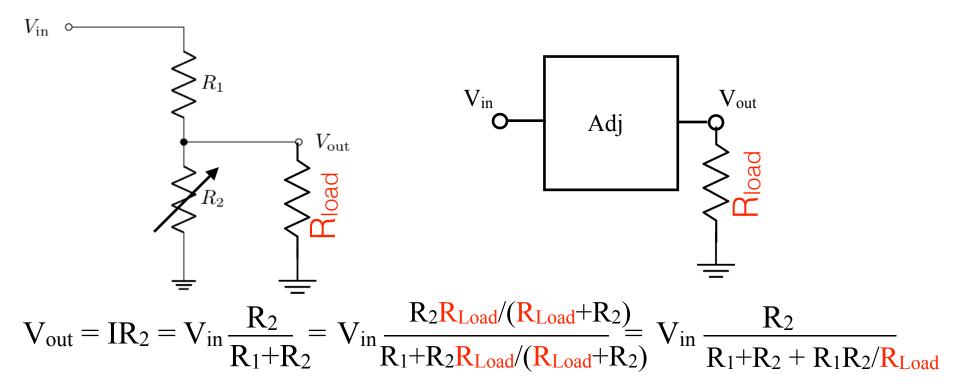


So we could use a voltage divider as a circuit stage that outputs an adjustable voltage. This could be the dimmer switch on a lamp.



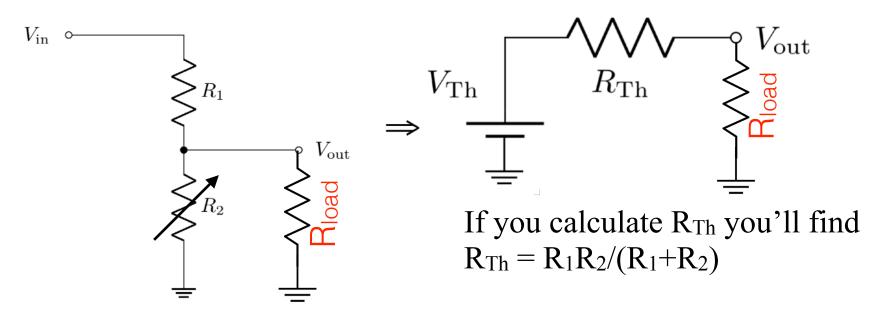
But, suppose I now connect this stage to the next stage in my circuit. In this case, it would be a lamp. That is the load.

So we could use a voltage divider as a circuit stage that outputs an adjustable voltage. This could be the dimmer switch on a lamp.



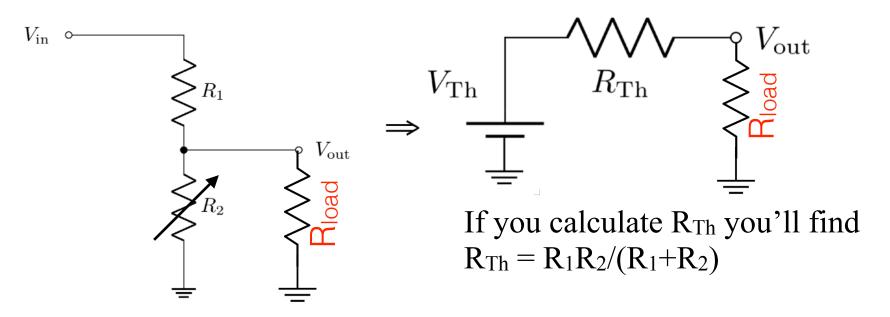
But, suppose I now connect this stage to the next stage in my circuit. In this case, it would be a lamp. That is the load. V_{out} is little changed by the load if $R_{Load} \gg R_1 R_2/(R_1+R_2)$.

Vout is little changed by the load if $R_{\text{Load}} \gg R_1 R_2 / (R_1 + R_2)$.



In general, the load causes negligible change to V_{out} wrt the stage's unloaded behavior **only if** $R_{Load} \gg R_{Th}$.

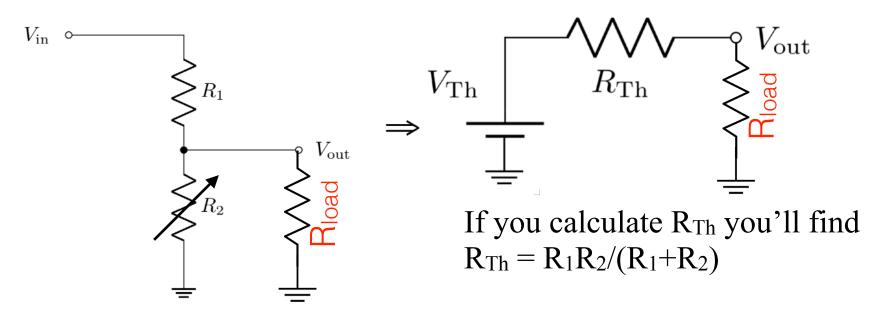
Vout is little changed by the load if $R_{\text{Load}} \gg R_1 R_2 / (R_1 + R_2)$.



In general, the load causes negligible change to V_{out} wrt the stage's unloaded behavior **only if** $R_{Load} \gg R_{Th}$.

Even more generally, we want the input resistance of the next stage to be much larger than the output resistance of this stage.

Vout is little changed by the load if $R_{\text{Load}} \gg R_1 R_2 / (R_1 + R_2)$.

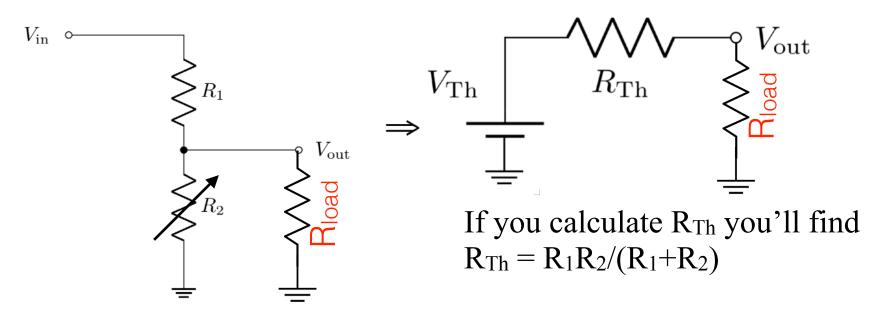


In general, the load causes negligible change to V_{out} wrt the stage's unloaded behavior **only if** $R_{Load} \gg R_{Th}$.

Even more generally, we want the input resistance of the next stage to be much larger than the output resistance of this stage.

Each stage should have large input resistance & small output resistance.

Vout is little changed by the load if $R_{\text{Load}} \gg R_1 R_2 / (R_1 + R_2)$.



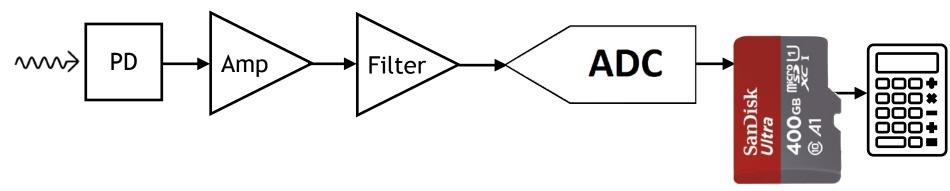
In general, the load causes negligible change to V_{out} wrt the stage's unloaded behavior **only if** $R_{Load} \gg R_{Th}$.

Even more generally, we want the input resistance of the next stage to be much larger than the output resistance of this stage.

Each stage should have large input impedance & small output impedance.

Chaining together stages for a measurement

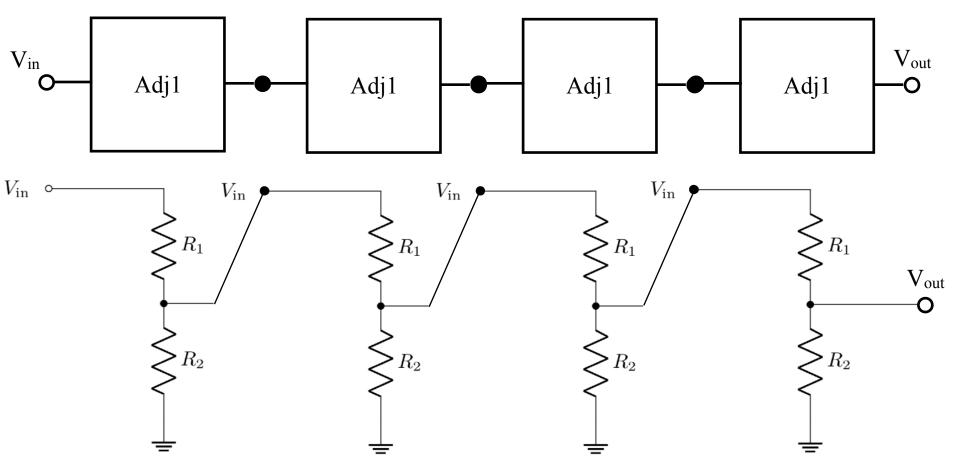
Each one of these stages should satisfy this rule, so I can chain them together without have any one affect the performance of its predecessor or successor.



We need each stage to have high input impedance and low output impedance to easily chain together multiple stages.

x10 rule

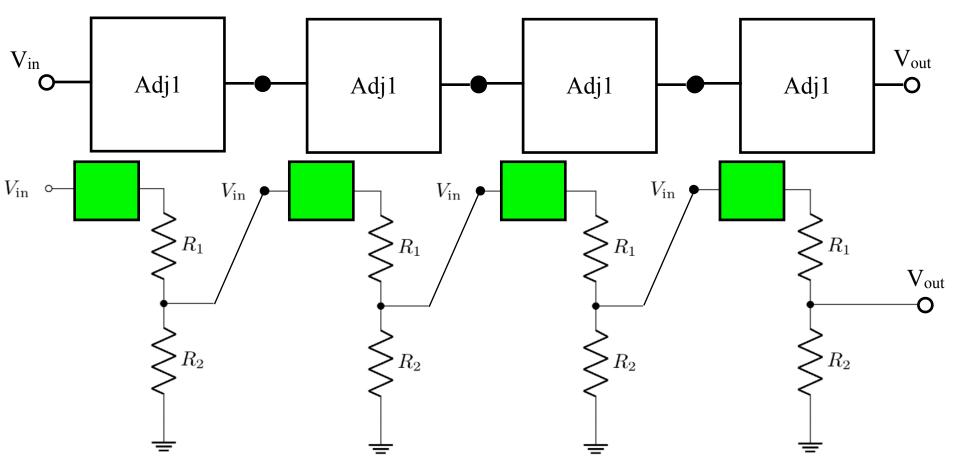
That looks hard with multiple stages.



I'd need each stage to have resistors 10 times as big as previous stage. That consumes high power in the early stages; $P = V^2/R$.

x10 rule

That looks hard with multiple stages.

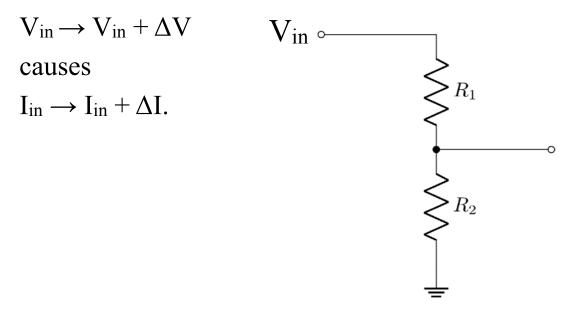


We need an "electromagical" impedance booster at the input of each stage We'll see how to do this soon, with a transistor.

- Rule for combining stages is that each stage should have high input impedance and low output impedance (resistance).
- How do we calculate these, and how do they differ?
- Use $R \equiv V/I$, or better $R \equiv \Delta V/\Delta I$.
- To increase the voltage by ΔV how much more current, ΔI , has to flow.

Input impedance

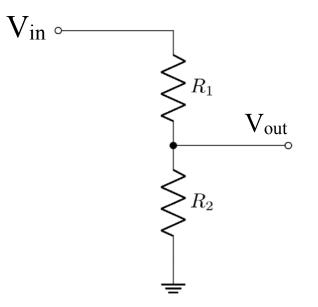
Use $R \equiv V/I$, or better $R \equiv \Delta V/\Delta I$. Increase V_{in} by ΔV ; then how much more current, ΔI_{in} , flows into the input.



 $I_{in} = V_{in}/(R_1+R_2)$ $\Delta I_{in} = \Delta V_{in}/(R_1+R_2)$ $\Delta V_{in}/\Delta I_{in} = R_1+R_2$ $R_{in} = R_1+R_2$ This is the two in series.

Output impedance

Use $R \equiv V/I$, or better $R \equiv \Delta V/\Delta I$. Increase V_{out} by ΔV ; then how much more current, ΔI_{out} , has to flow into the output.



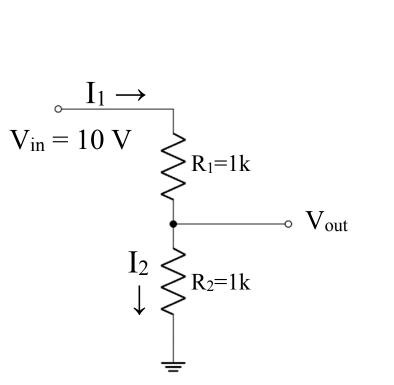
Output impedance

Use $R \equiv V/I$, or better $R \equiv \Delta V/\Delta I$. Increase V_{out} by ΔV ; then how much more current, ΔI_{out} , has to flow into the output.

Illustrate with a numeric example, forcing V_{out} .

Find how changing $V_{out} \rightarrow V_{out} + \Delta V$ changes $I_{out} \rightarrow I_{out} + \Delta I_{.}$

What are I₁, I₂, and V_{out}?

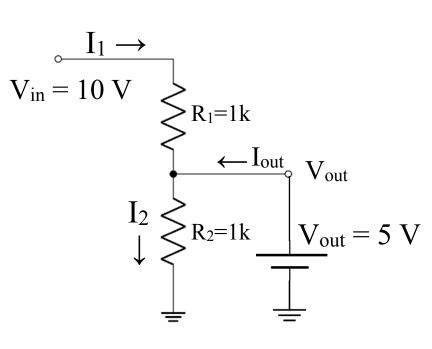


Output impedance

Use $R \equiv V/I$, or better $R \equiv \Delta V/\Delta I$. Increase V_{out} by ΔV ; then how much more current, ΔI_{out} , has to flow into the output.

Illustrate with a numeric example, forcing V_{out}.

Find how changing $V_{out} \rightarrow V_{out} + \Delta V$ changes $I_{out} \rightarrow I_{out} + \Delta I$.



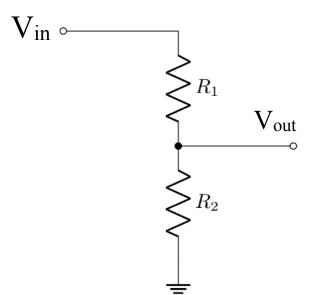
What are I_1 , I_2 , and I_{out} ? $I_{out}=0$, and $I_1 = I_2 = 10/2000=5$ mA. Change V_{out} to 6 V, i.e. $\Delta V=1$, now what are I_1 , I_2 , and I_{out} ? $I_{2} \neq R_{2}=1k$ $V_{out} = 5 V$ $I_{1} R_{1} = 10-6 = 4, \text{ so } I_{1} = 4 \text{ mA.}$ $I_{2} R_{2} = 6-0 = 6, \text{ so } I_{2} = 6 \text{ mA.}$ $I_{out} = 2 \text{ mA, } \Delta V / \Delta I = 1 V / 2 \text{ m}$ This is $R_{1} \parallel R_{2}$. I_{out} is no longer 0. Find it from $I_2 = I_1 + I_{out}$. Calculate $I_1 \& I_2$ using Ohm's law. $I_{out} = 2 \text{ mA}, \Delta V / \Delta I = 1 V / 2 \text{ mA} = 500 \Omega.$

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 R_{in} = effective resistance looking into input.

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.



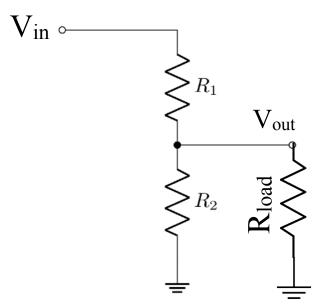
 R_{in} = one path through R_1 then R_2 in series. $R_{in} = R_1 + R_2$.

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 R_{in} = effective resistance looking into input.

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.



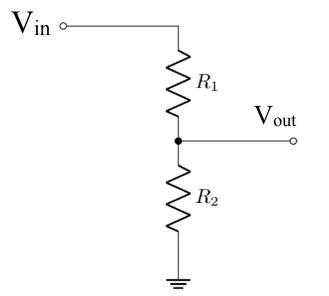
 $R_{in} = \text{one path through } R_1 \text{ then two } \| \text{ paths.}$ $R_{in} = R_1 + R_2 \| R_{\text{Load}} \cong R_1 + R_2, \text{ if } R_{\text{Load}} \text{ is big.}$ $R_{in} \cong R_1 + R_2, \text{ if } R_{\text{Load}} \text{ is big.}$

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 R_{in} = effective resistance looking into input.

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.



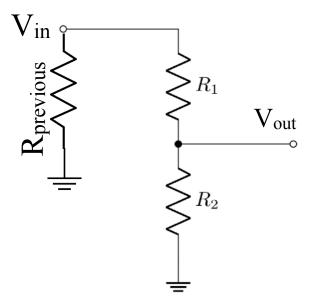
$$\begin{aligned} R_{out} &= path \ 1 \ \underline{or} \ path \ 2 \\ R_{out} &= path \ 1 \ \| \ path \ 2 \\ R_{out} &= R_1 \ \| \ R_2. \end{aligned}$$

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 $R_{in} = effective resistance looking into input.$

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.



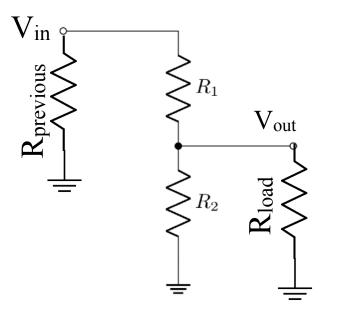
$R_{out} = path 1 \underline{or} path 2$	
R _{out} = path 1 ∥ path 2	
$\mathbf{R}_{\text{out}} = \mathbf{R}_1 \parallel \mathbf{R}_2.$	
$\mathbf{R}_{\text{out}} = (\mathbf{R}_1 + \mathbf{R}_{\text{previous}}) \ \mathbf{R}_2.$	
$R_{out} \cong R_1 \parallel R_2$ if $R_{previous}$ is small	1

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 $R_{in} = effective resistance looking into input.$

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.



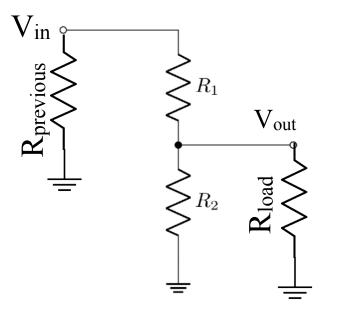
 $R_{in} \cong R_1 + R_2$, if R_{Load} is big. $R_{out} \cong R_1 \parallel R_2$ if $R_{previous}$ is small.

The formal definition is $R=\Delta V/\Delta I$, but we can use a simpler approach, illustrated by the example, where we found Rin = R_1+R_2 & Rout = $R_1|R_2$

 R_{in} = effective resistance looking into input.

 $R_{out} = effective resistance looking into output.$

Trace current path from input or output terminal to all fixed voltage points.

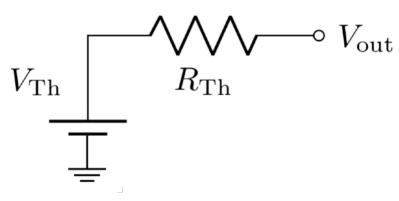


 $R_{in} \cong R_1 + R_2$, if R_{Load} is big. $R_{out} \cong R_1 \parallel R_2$ if $R_{previous}$ is small. Design to have big $R_{Load} = R_{in}$ of next stage and small $R_{previous} = R_{out}$ of previous stage. Then they won't impact ability to get a big R_{in} and small R_{out} for this stage.

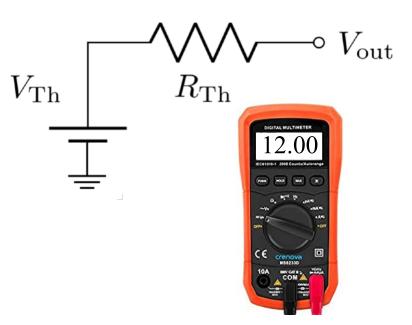
We will eventually see how to make $R_{in} \rightarrow \infty$ and $R_{out} \rightarrow 0$.

Ideal voltage and current sources

In the Thevenin equivalent circuit, we treated V_{Th} as a battery.



Batteries have a set EMF. Ideally a 12V battery will always give 12V output. But what happens when it discharges?

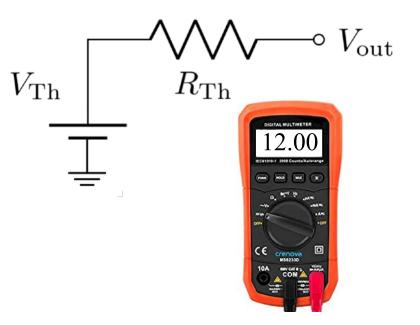


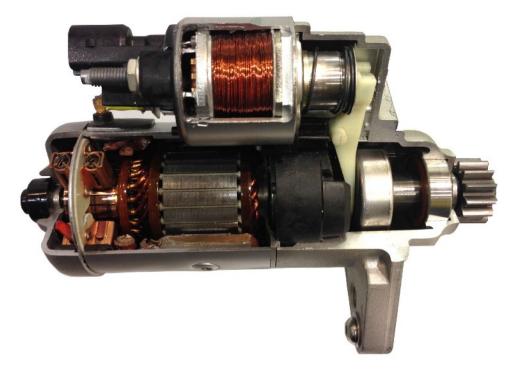
Ideal voltage and current sources

In the Thevenin equivalent circuit, we treated V_{Th} as a battery.

 V_{Th} R_{Th} V_{out} Batteri Ideally give 12 when i

Batteries have a set EMF. Ideally a 12V battery will always give 12V output. But what happens when it discharges?



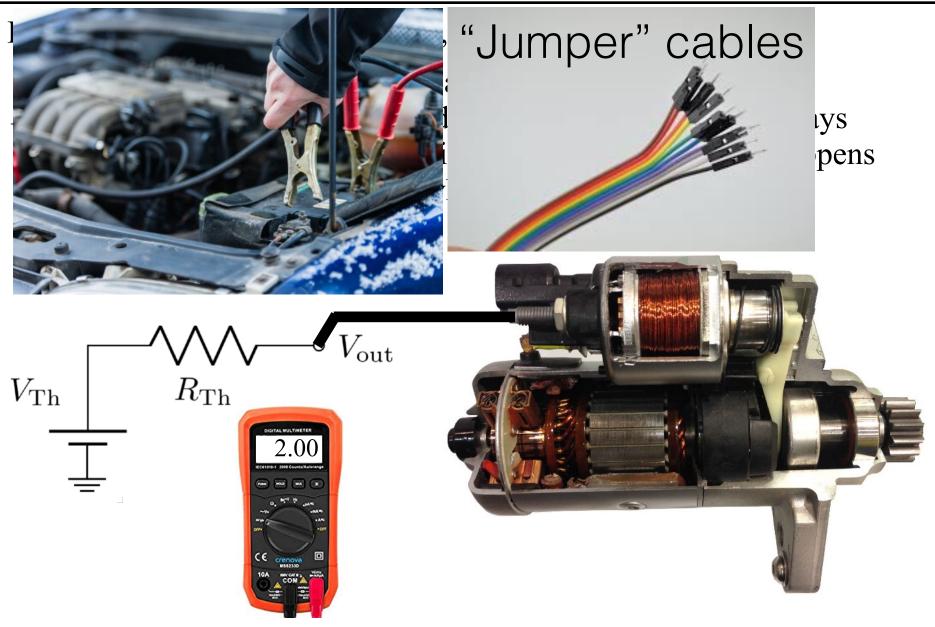


Ideal voltage and current sources

In the Thevenin equivalent circuit, we treated V_{Th} as a battery.

Batteries have a set EMF. $\multimap V_{\rm out}$ Ideally a 12V battery will always V_{Th} R_{Th} give 12V output. But what happens when it discharges? \int_{Out} R_{Th} $V_{\rm Th}$

Ideal voltage and current sources

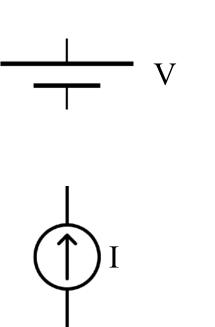


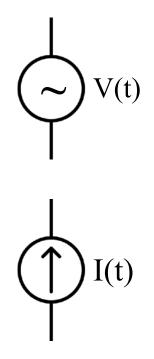
AC/DC and signals

The signals we are interested in measuring are usually time dependent, rather than some constant voltage.

Constant voltage & current sources.

Alternating voltage & current sources.

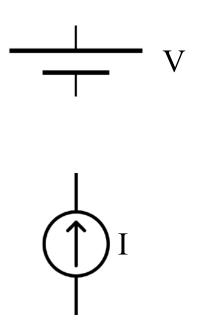




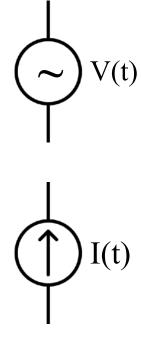
AC/DC and signals

The signals we are interested in measuring are usually time dependent, rather than some constant voltage.

- Constant voltage & current sources.
- Direct current (DC)



- Alternating voltage & current sources.
- Alternating current (AC)



AC signals can be sine waves, or anything

Sine wave:

 $V(t) = A \sin(2\pi f t) + V_0$ $V(t) = A \sin(\omega t) + V_0$

Square wave

Triangle wave

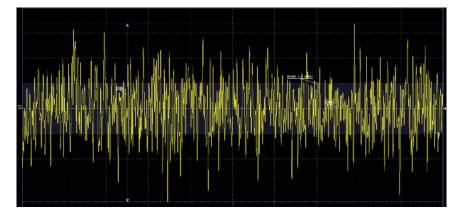
Sawtooth

Pulse

General variation

Noise (1/f noise has same power/Hz)

We'll typically deal with sine wave signals, because any wave can be treated as a Fourier sum of them.



Parameters of a sine wave

Sine wave:

 $V(t) = A \sin(2\pi f t) + V_0$ $V(t) = A \sin(\omega t) + V_0$

We'll typically deal with sine wave signals, because any wave can be treated as a Fourier sum of them.

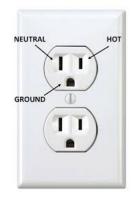
Amplitude often specified as $V_{RMS} = A/\sqrt{2}$

This is what matters most for power consumption.

 $P = IV = V^2/R$

and average of \sin^2 is 1/2.

Electrical power in your house is 120 V RMS, so A=170 V.



Ratios of signals and decibels

The ratio of two AC signals is often described in decibels, which you probably learned about for sound waves.

 $1 \text{ dB} = 20 \log (A_2/A_1)$

+6 dB if $A_2 = 2A_1$ +20 dB if $A_2 = 10A_1$

-20 dB if $A_2 = A_1/10$

Common to compare power levels, and $P \propto V^2$, so 1 dB = 10 log (P₂/P₁)

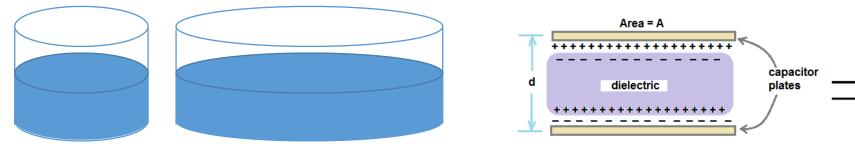
-3 dB corresponds to half the power, or A/sqrt(2)

Capacitors

Now we get to introduce a new circuit element, which is manifestly AC.

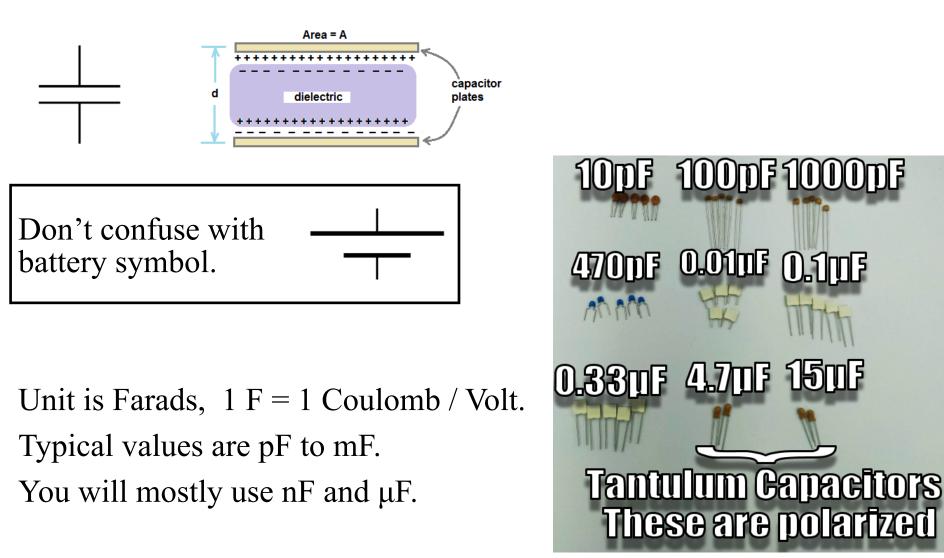
- A capacitor stores charge, producing an electric field and hence energy. V = q/C, which I remember more easily as q = CV.
- In the water analogy, a water storage tank is a capacitor.
- A wider tank has more capacity, ie more water (q) can be stored for the same height (V).





Capacitor symbol

Circuit symbol matches the visualization of a parallel plate capacitor.



100pF1000pF

Olime

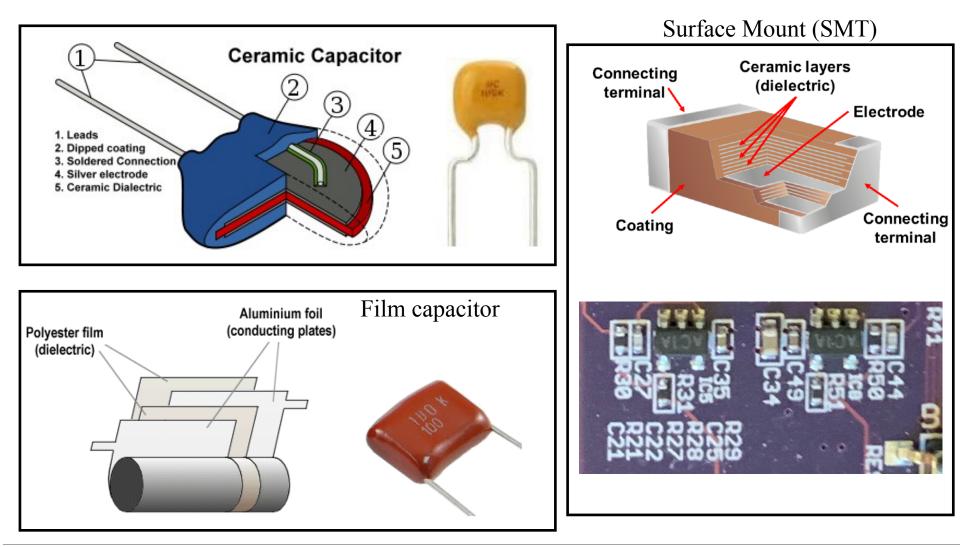
15015

These are polarized

0.0105

Capacitor construction

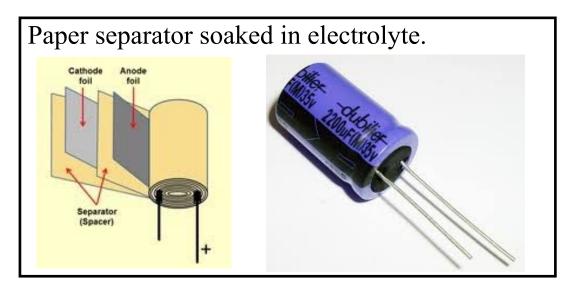
Film capacitors and ceramic are common for C < 1μ F.



Phys127AL Lecture 2: Calculating input & output impedance, AC signals, capacitors

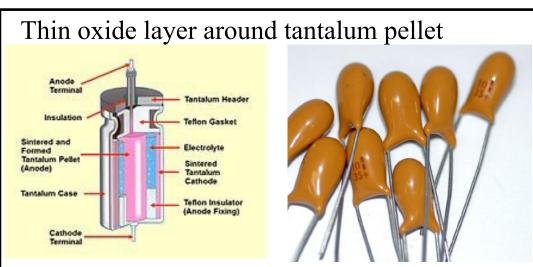
Capacitor construction

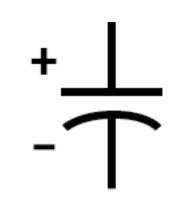
Electrolytic and tantalum capacitors are common for $C > 1 \mu F$.



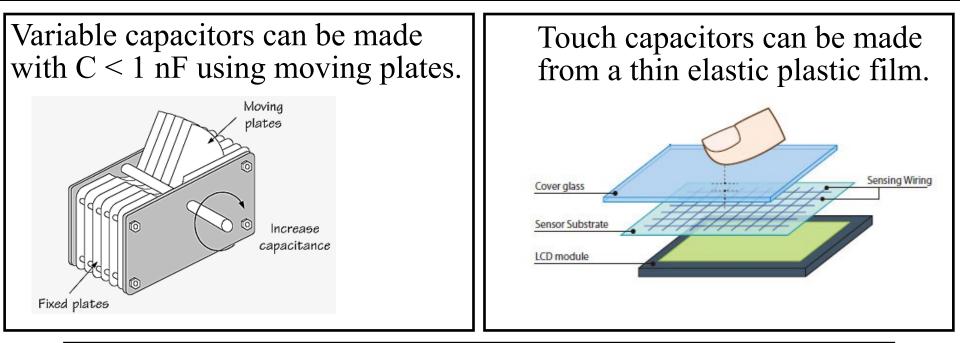
Use of an electrolyte makes these only work if polarity maintained.

So they have a different symbol.

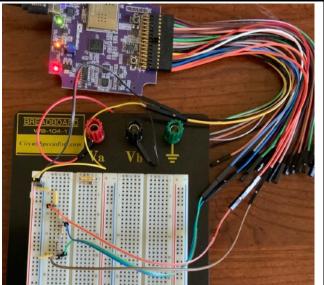




Other capacitor types



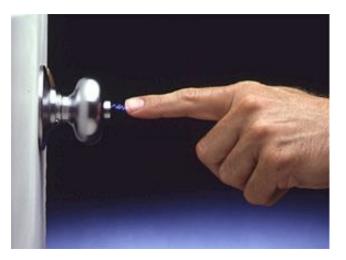
Parasitic capacitance is produced when any two conductors pass near each other. Just jostling your wires can change the capacitance in your circuit. Even moving your finger near a pair of wires.



Electrostatic discharge

Any single conductor has capacitance; the other electrode is the earth.

You have capacitance, but not very large. Adding electrostatic charge to you, by rubbing feet on a carpet, gives you are large voltage through V = q/C, even with a relative small charge.



Electrostatic discharge

Any single conductor has capacitance; the other electrode is the earth.

You have capacitance, but not very large. Adding electrostatic charge to you, by rubbing feet on a carpet, gives you are large voltage through V = q/C, even with a relative small charge.

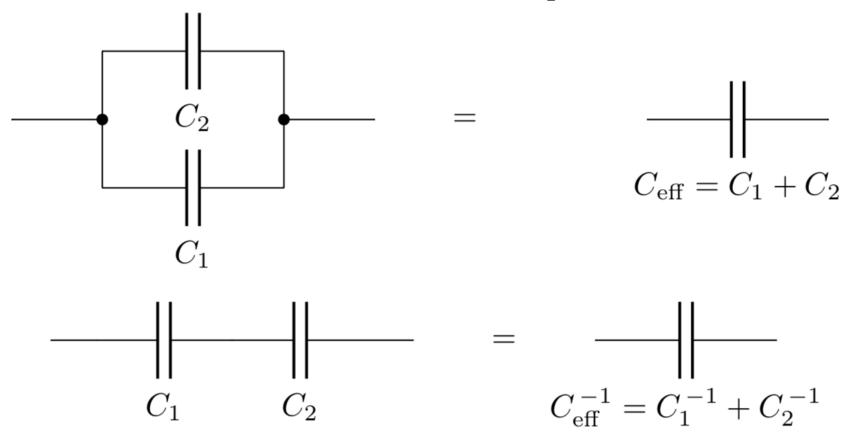


DavidStuart@UCSB.edu

Phys127AL Lecture 2: Calculating input & output impedance, AC signals, capacitors

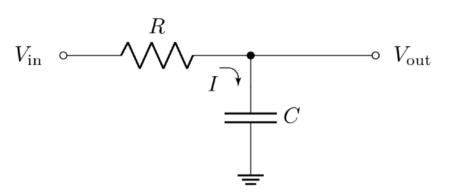
Combining capacitors

Capacitance values add in series and parallel opposite to the way resistors do. But it is intuitive: two tanks in parallel hold more water.

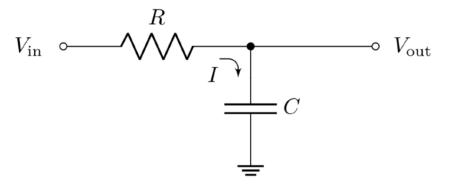


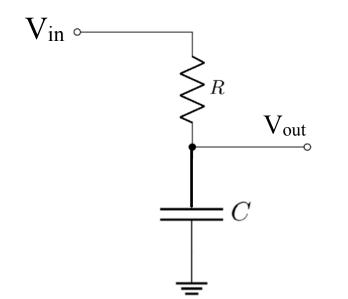
You can derive these from q = CV, and Kirchoff's laws.

Suppose we charge a capacitor through a resistor with this circuit.

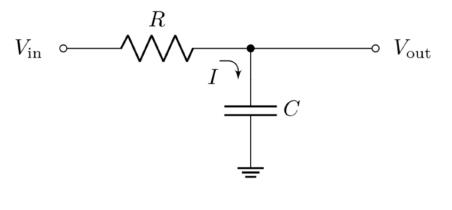


Suppose we charge a capacitor through a resistor with this circuit.



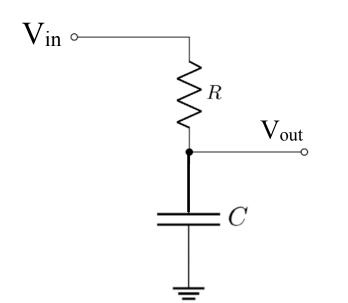


Suppose we charge a capacitor through a resistor with this circuit.

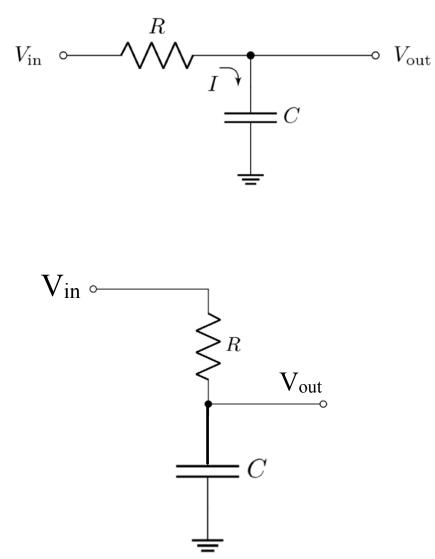


We can analyze this from $q = CV \implies I = C dV/dt$

I *through* capacitor is related to the change in the voltage *across* the capacitor.



Suppose we charge a capacitor through a resistor with this circuit.



We can analyze this from

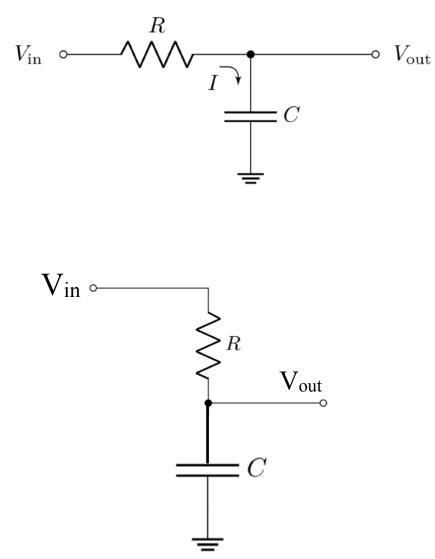
$$q = CV \implies I = C dV/dt$$

I *through* capacitor is related to the change in the voltage *across* the capacitor.

The voltage across the capacitor is V_{out} .

The current through the capacitor is whatever current is flowing through R from V_{in} , which is the voltage *dropped across* R:

Suppose we charge a capacitor through a resistor with this circuit.



We can analyze this from

$$q = CV \implies I = C dV/dt$$

I *through* capacitor is related to the change in the voltage *across* the capacitor.

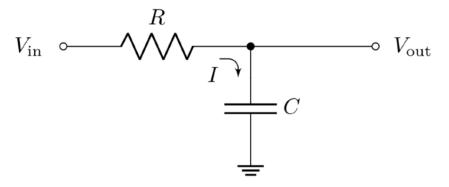
The voltage across the capacitor is V_{out} .

The current through the capacitor is whatever current is flowing through R from V_{in}, which is the voltage *dropped across* R:

 $I = (V_{in}\text{-}V_{out})/R = C \ dV_{out}/dt$

Note that this assumes V_{out} is connected to a high input resistance.

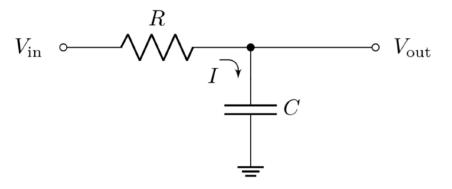
Suppose we charge a capacitor through a resistor with this circuit.



 $I = (V_{in}-V_{out})/R = C dV_{out}/dt$ V_{out} is the time varying voltage, so just call it V(t), our variable in this DE. $(V_{in}-V)/R = C dV/dt$ Suppose V_{in} is a step function at t=0.

Separate variables and we get $dt/RC = dV/(V_{in}-V) = -dV/(V-V_{in})$

Suppose we charge a capacitor through a resistor with this circuit.



$$I = (V_{in}-V_{out})/R = C dV_{out}/dt$$

V_{out} is the time varying voltage, so just
call it V(t), our variable in this DE.
(V_{in}-V)/R = C dV/dt

114

Suppose V_{in} is a step function at t=0.

Separate variables and we get $dt/RC = dV/(V_{in}-V) = -dV/(V-V_{in})$ Integrate both sides from t=0 to t=t and $V=V_0=V(t=0)$ to V=V(t).

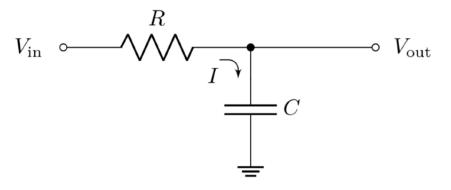
$$\int_{0}^{t} dt'/RC = -\int_{V_0}^{V} dV'/(V'-V_{in}) \implies t/RC = -\ln[(V-V_{in})/(V_0-V_{in})]$$

$$(V-V_{in}) = (V_0-V_{in}) e^{-t/RC} \implies V = V_{in} + (V_0-V_{in}) e^{-t/RC}$$

If V₀=0, we get V(t) = V_{in} (1-e^{-t/RC})

Discharging a capacitor

Suppose we charge a capacitor through a resistor with this circuit.



$$V_{out}$$
 is the time varying voltage, so just
call it V(t), our variable in this DE.
 $(V_{in}-V)/R = C dV/dt$
Suppose V_{in} is a step function at t=0.

 $I = (V \cdot V) / D = C dV / dt$

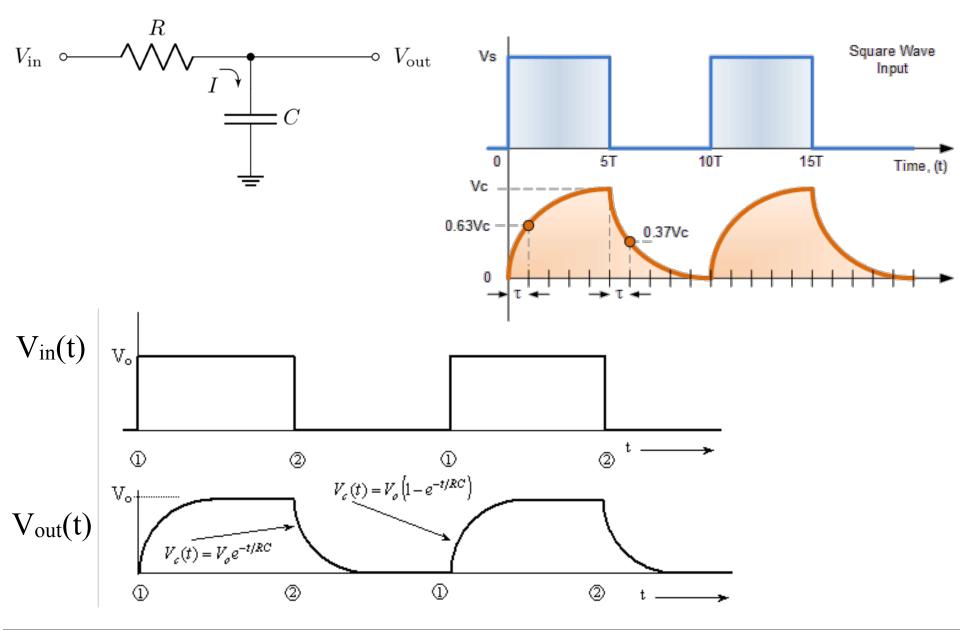
Separate variables and we get $dt/RC = dV/(V_{in}-V) = -dV/(V-V_{in})$ Integrate both sides from t=0 to t=t and V=V₀=V(t=0) to V=V(t).

$$\int_{0}^{t} dt'/RC = -\int_{V_0}^{V} dV'/(V'-V_{in}) \implies t/RC = -\ln[(V-V_{in})/(V_0-V_{in})]$$

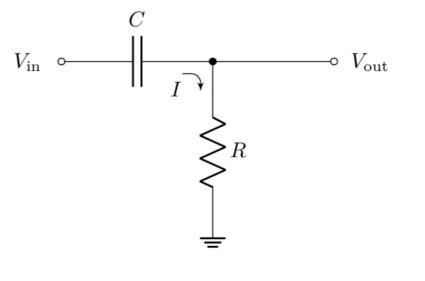
$$(V-V_{in}) = (V_0-V_{in}) e^{-t/RC} \implies V = V_{in} + (V_0-V_{in}) e^{-t/RC}$$

Now we get $V(t) = V_0 e^{-t/RC}$

Square wave input to an RC circuit



Differentiator



We can again analyze this from

$$q = CV \implies I = C dV/dt$$

I *through* capacitor is related to the change in the voltage *across* the capacitor.

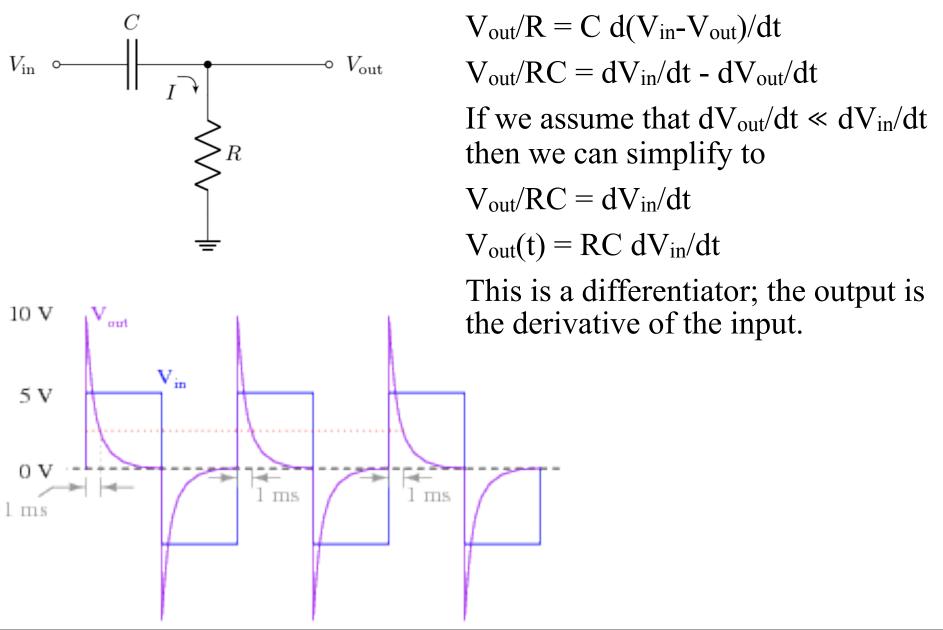
The voltage across the capacitor is V_{in} - V_{out} .

The current through the capacitor is whatever current is flowing through R from V_{out}, which is the voltage *dropped across* R:

 $I = V_{out}/R = C d(V_{in}-V_{out})/dt$

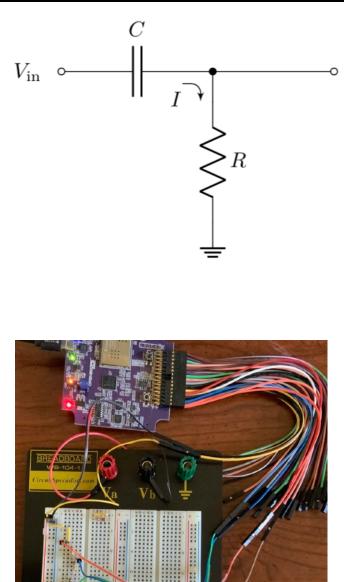
Note that this assumes V_{out} is connected to a high input resistance.

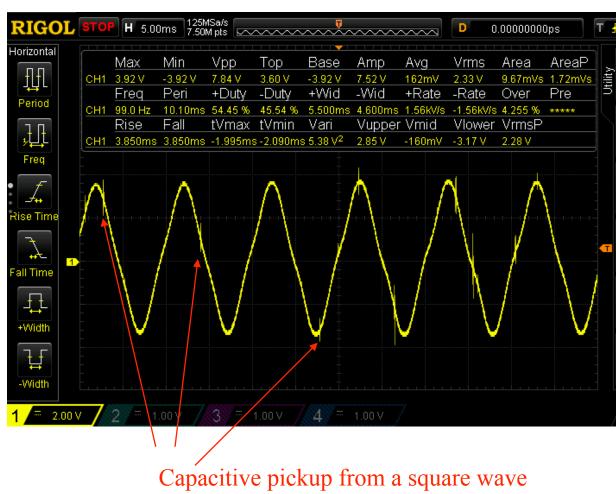
Differentiator



Differentiator pickup

 $V_{\rm out}$





DavidStuart@UCSB.edu

Phys127AL Lecture 2: Calculating input & output impedance, AC signals, capacitors

Ohm's law for capacitors

- We can find an IV relationship for a capacitor. Let's assume that V(t) is sinusoidal; we can then form any AC signal from a Fourier sum of these.
- I'll actually use a cosine for reasons that will become clear later.
- Suppose the voltage across the capacitor is

 $V(t) = V_0 \cos \omega t$

Then the current through it is

 $I(t) = C dV(t)/dt = -\omega CV_0 \sin \omega t$

So we have a relation between the magnitudes of V and I

$$|\mathbf{V}| = |\mathbf{I}| (1/\omega \mathbf{C})$$

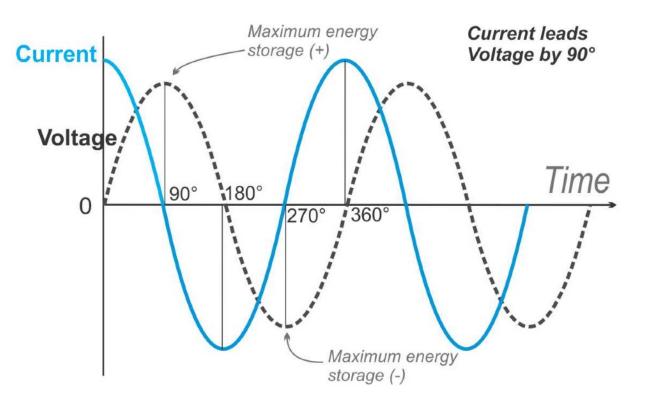
This is similar to Ohm's law, and we can identify $1/\omega C$ as being like the "resistance of a capacitor". But it is not the full story because the *phase* of the current differs from the phase of the voltage.

Ohm's law for capacitors

 $|\mathbf{V}| = |\mathbf{I}| (1/\omega \mathbf{C})$

This is similar to Ohm's law, and we can identify $1/\omega C$ as being like the "resistance of a capacitor". But it is not the full story because the *phase* of the current differs from the phase of the voltage.

Ideal Capacitive Circuit Phase Angle



This diagram has V(t) as a sine not a cosine, but just shift time.

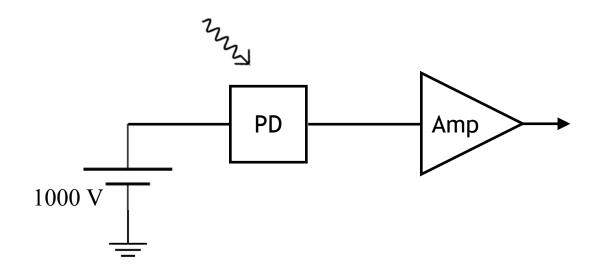
Ohm's law for capacitors

 $|\mathbf{V}| = |\mathbf{I}| (1/\omega \mathbf{C})$

- This is similar to Ohm's law, and we can identify $1/\omega C$ as being like the "resistance of a capacitor". But it is not the full story because the *phase* of the current differs from the phase of the voltage.
- Since the voltage "reacts to the current", and vice versa, this is called *reactance* rather than resistance.
- The more general term is *impedance*, which encompasses both resistance and reactance. Impedance is the term to use for both henceforth.
- So the impedance of a capacitor is $1/\omega C$.
- The minus sign indicates the phase information; though a rigorous treatment of that is more complex as we will see soon.
- The $1/\omega C$ means that the impedance of a capacitor depends on the frequency of the signal.
 - Low impedance for high frequency AC and high impedance for DC.

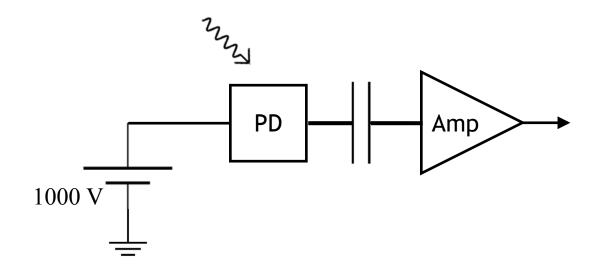
DC blocking capacitors

The infinite resistance at DC is used to block DC from one stage of a circuit reaching another stage.



DC blocking capacitors

The infinite resistance at DC is used to block DC from one stage of a circuit reaching another stage.



In addition to a capacitance value, you will find a voltage rating on capacitors indicating how much they can stand off.

Expressing AC signals in complex notation

It simplifies the handling of AC signals to treat them with complex notation. We can do this with Euler's formula.

 $e^{i\theta} = \cos\,\theta + i\,\sin\,\theta$

So we can express $V(t) = V_0 \cos \omega t$ as $V(t) = V_0 e^{i\omega t}$ well the real part is V(t). We already use *i* for a small signal change in current, so in electronics we instead use $j^2 = -1$. (Textbook uses *j*=-*i*). So we'll represent the voltage as $\widetilde{V}(t) = V_0 e^{j\omega t}$

The tilde reminds us that this is the complex representation. Now calculate the current from I = C dV/dt.

$$\widetilde{\mathbf{I}} = \mathbf{C} j \boldsymbol{\omega} \mathbf{V}_0 \, \mathbf{e}^{j \boldsymbol{\omega} \mathbf{t}} = j \boldsymbol{\omega} \mathbf{C} \widetilde{\mathbf{V}}$$

So, we can write an Ohm's law like relation between V and I:

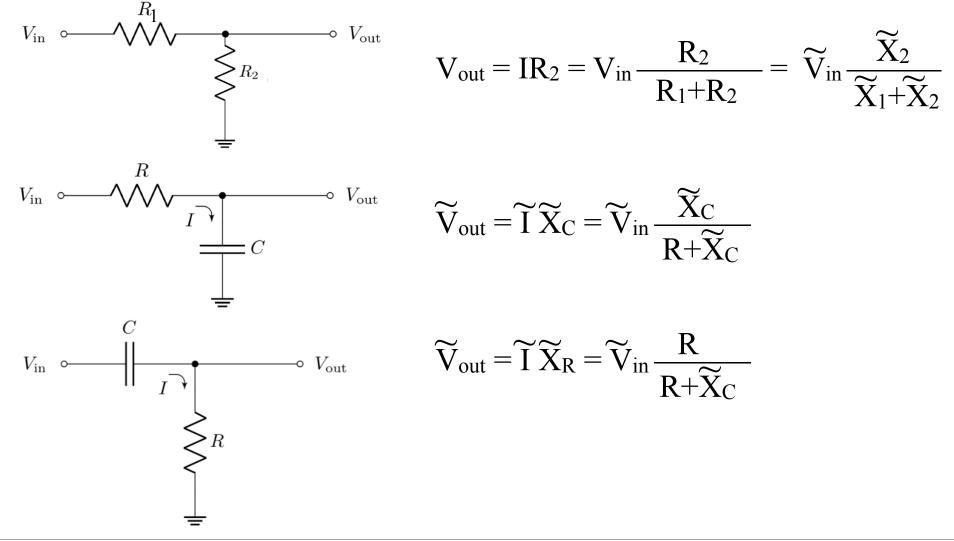
$$\widetilde{\mathbf{V}} = \widetilde{\mathbf{I}} (1/j\omega \mathbf{C}) = \widetilde{\mathbf{I}} (-j/\omega \mathbf{C}) \implies \widetilde{\mathbf{V}} = \widetilde{\mathbf{I}} \widetilde{\mathbf{X}}_{\mathbf{C}} \quad \mathbf{cf} \quad \widetilde{\mathbf{V}} = \widetilde{\mathbf{I}} \widetilde{\mathbf{X}}_{\mathbf{R}}$$

Where the impedance of the capacitor in complex representation is $\widetilde{X}_C = -j/\omega C$ of $\widetilde{X}_R = R$

Expressing AC signals in complex notation

This will simplify handling a mix of capacitors and resistors.

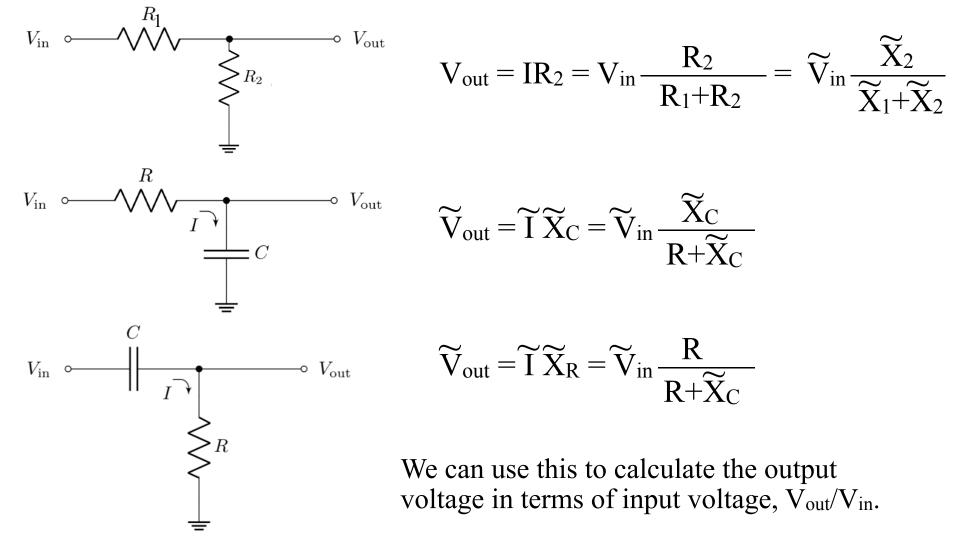
This makes the circuits below just complex voltage dividers.

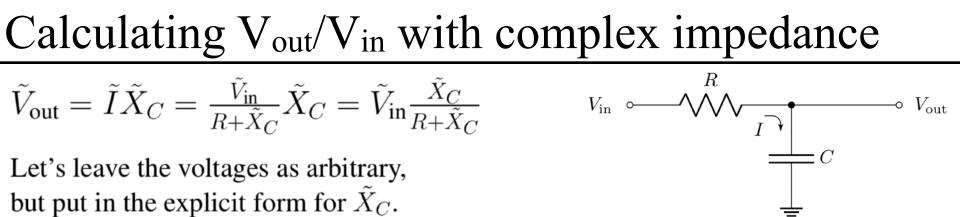


Expressing AC signals in complex notation

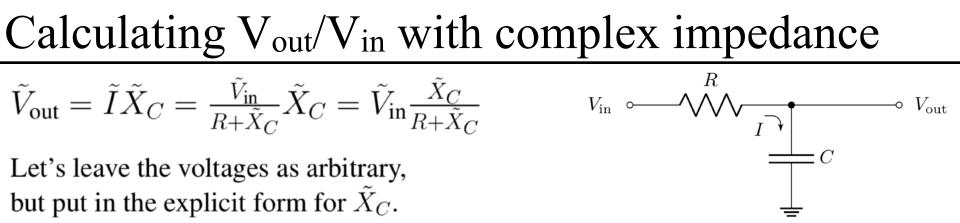
This will simplify handling a mix of capacitors and resistors.

This makes the circuits below just complex voltage dividers.





$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right]$$



$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$

Calculating V_{out}/V_{in} with complex impedance $\tilde{V}_{out} = \tilde{I}\tilde{X}_C = \frac{\tilde{V}_{in}}{R+\tilde{X}_C}\tilde{X}_C = \tilde{V}_{in}\frac{\tilde{X}_C}{R+\tilde{X}_C}$ $V_{in} \sim \sqrt{N}_{I} \sim \sqrt{N}_{I} \sim V_{out}$ Let's leave the voltages as arbitrary, but put in the explicit form for \tilde{X}_C .

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2}$$

$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2}$$
$$\tilde{V}_{\text{out}} = \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2}$$

$$|\tilde{V}_{\text{out}}| = |\tilde{V}_{\text{in}}| \left| \frac{1 - j\omega RC}{1 + \omega^2 R^2 C^2} \right|$$

$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \left|\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right|$$

Calculating V_{out}/V_{in} with complex impedance

$$\tilde{V}_{out} = \tilde{I}\tilde{X}_C = \frac{\tilde{V}_{in}}{R+\tilde{X}_C}\tilde{X}_C = \tilde{V}_{in}\frac{\tilde{X}_C}{R+\tilde{X}_C}$$
 $V_{in} \sim \sqrt{N}_{I} \sim \sqrt{N}_{I} \sim V_{out}$
Let's leave the voltages as arbitrary,
but put in the explicit form for \tilde{X}_C .

$$\begin{split} \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] = \tilde{V}_{\text{in}} \left[\frac{-j/\omega C}{R - j/\omega C} \right] \left[\frac{R + j/\omega C}{R + j/\omega C} \right] = \tilde{V}_{\text{in}} \frac{-jR/\omega C - j^2/\omega^2 C^2}{R^2 - j^2/\omega^2 C^2} \\ \tilde{V}_{\text{out}} &= \tilde{V}_{\text{in}} \frac{1/\omega^2 C^2 - jR/\omega C}{R^2 + 1/\omega^2 C^2} * \left[\frac{\omega^2 C^2}{\omega^2 C^2} \right] = \tilde{V}_{\text{in}} \frac{1 - j\omega R C}{1 + \omega^2 R^2 C^2} \end{split}$$

$$|\tilde{V}_{\text{out}}| = |\tilde{V}_{\text{in}}| \left| \frac{1 - j\omega RC}{1 + \omega^2 R^2 C^2} \right|$$

$$\frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \left|\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right| = \sqrt{\left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right] \left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right]^*} = \sqrt{\left[\frac{1-j\omega RC}{1+\omega^2 R^2 C^2}\right] \left[\frac{1+j\omega RC}{1+\omega^2 R^2 C^2}\right]} \\ \frac{|\tilde{V}_{\text{out}}|}{|\tilde{V}_{\text{in}}|} = \sqrt{\frac{1+\omega^2 R^2 C^2}{(1+\omega^2 R^2 C^2)^2}} = \frac{\sqrt{1+\omega^2 R^2 C^2}}{1+\omega^2 R^2 C^2} = \frac{1}{\sqrt{1+\omega^2 R^2 C^2}}$$

This is the response function for the circuit, and it is frequency dependent through $\omega = 2\pi f$.